

### 1. Problem and Aims:

- Bischofite is normally extracted from the subsurface by solution mining in underground caverns.
- Abandonment of the caverns causes the wall rock to creep towards the inside due to overburden stress, which in turn results in subsidence at the surface.
- Aim: Flow law that allows reliable extrapolation from lab to strain rate  $\sim 10^{-9} \text{ s}^{-1}$ , to be used in modelling.

### 2. Material and experiments:

- Polycrystalline cylindrical samples with average length = 80 mm and diameter = 35 mm (Figure 1)
- From as received cores (Figure 2)
- Jacketed and undried
- Triaxial deformation apparatus at HPT Lab (Figure 3)
- Triaxial tests at real *in-situ* conditions:  $T = 70^\circ\text{C}$ ,  $P_c = 40 \text{ MPa}$ . Additional tests at  $P_c = 70 \text{ MPa}$ .
- Strain rate stepping experiments with stress relaxation after every constant deformation step



Figure 1. Bischofite sample with piston assembly

Figure 2. As received 100 cm long pure bischofite core



Figure 3. Triaxial apparatus (Shuttle vessel)

### 4. Flow laws used in analyses (at constant Temperature):

$$\dot{\epsilon} = A\sigma^n \quad (\text{Grain Size Insensitive (GSI) Power law})$$

$$\dot{\epsilon} = A'\sigma^n \exp\left(\frac{\sigma}{B}\right) \quad (\text{GSI Exponential law})$$

$$\dot{\epsilon} = C\sigma d^{-p} \quad (\text{Grain Size Sensitive})$$

### 5. Role of grain size:

- From previous work (Van Eekelen et al (1984): Bischofite shows dynamic recrystallization.
- Grain sizes at steady state stresses (our experiments) from piezometric relation Figure 10.

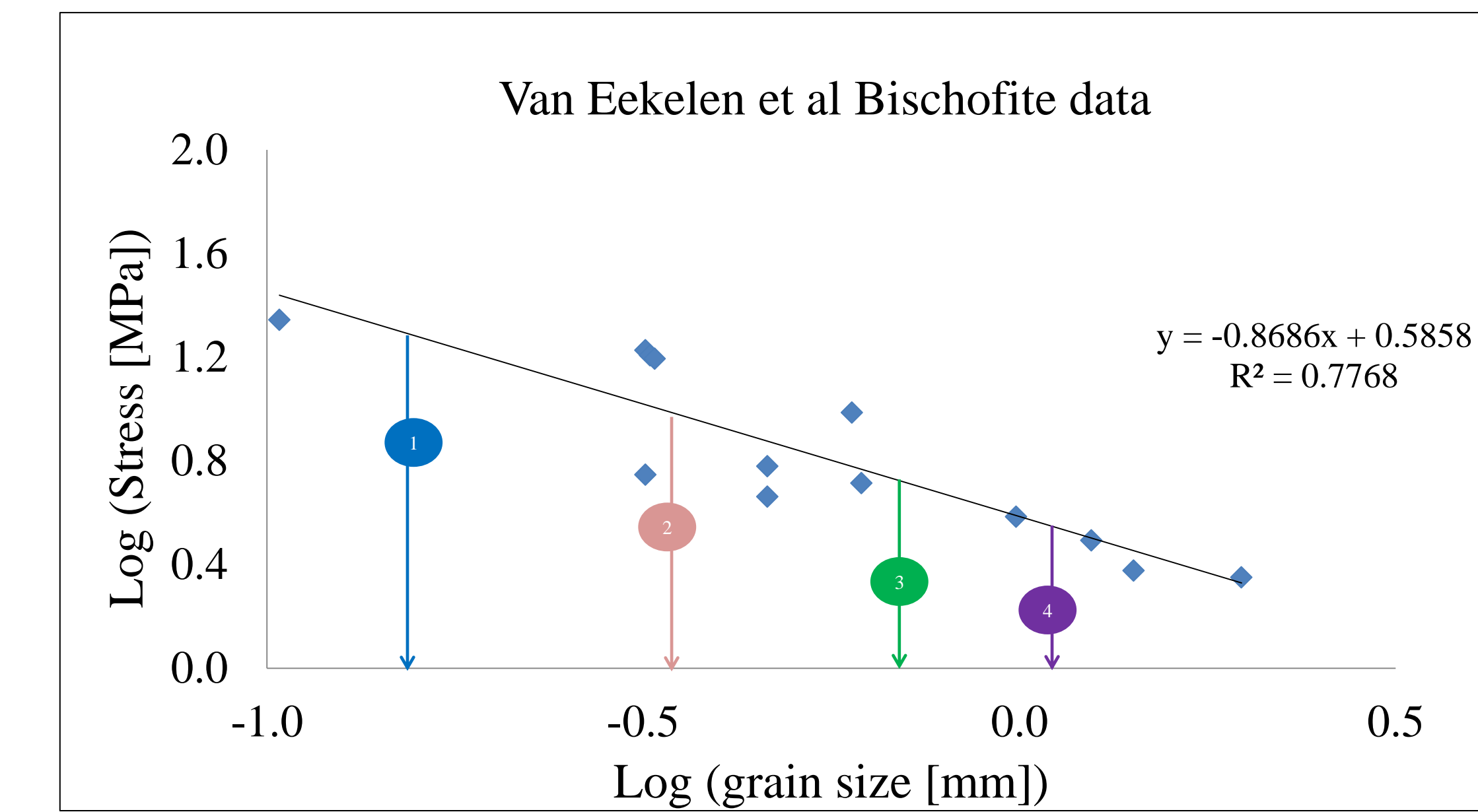


Figure 10. Flow stress vs. mean grain size at 60°C

- Relaxation trend towards  $n = 1$ , suggests role of GSS
- So description by composite flow law (GSI+GSS)?  $\dot{\epsilon} = A\sigma^n \exp\left(\frac{\sigma}{B}\right) + C\sigma d^{-p}$ ,
- Evaluation of 'p' based on assumption of constant microstructure (constant grain size) during relaxation.
- Result:  $p = 2-0.6$ : No conclusion yet on mechanism

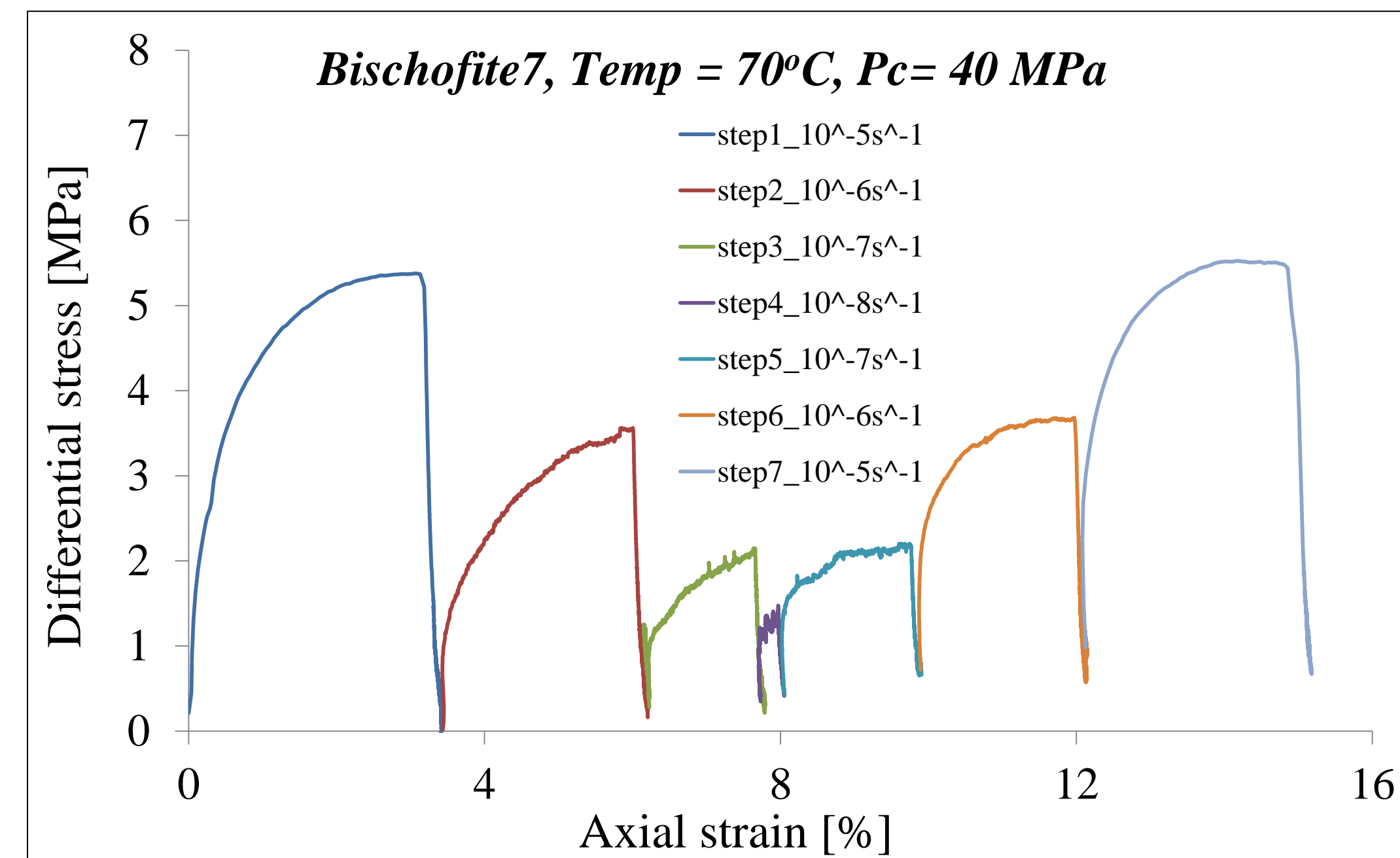


Figure 4. Strain rate sensitivity of flow stress at 40 MPa

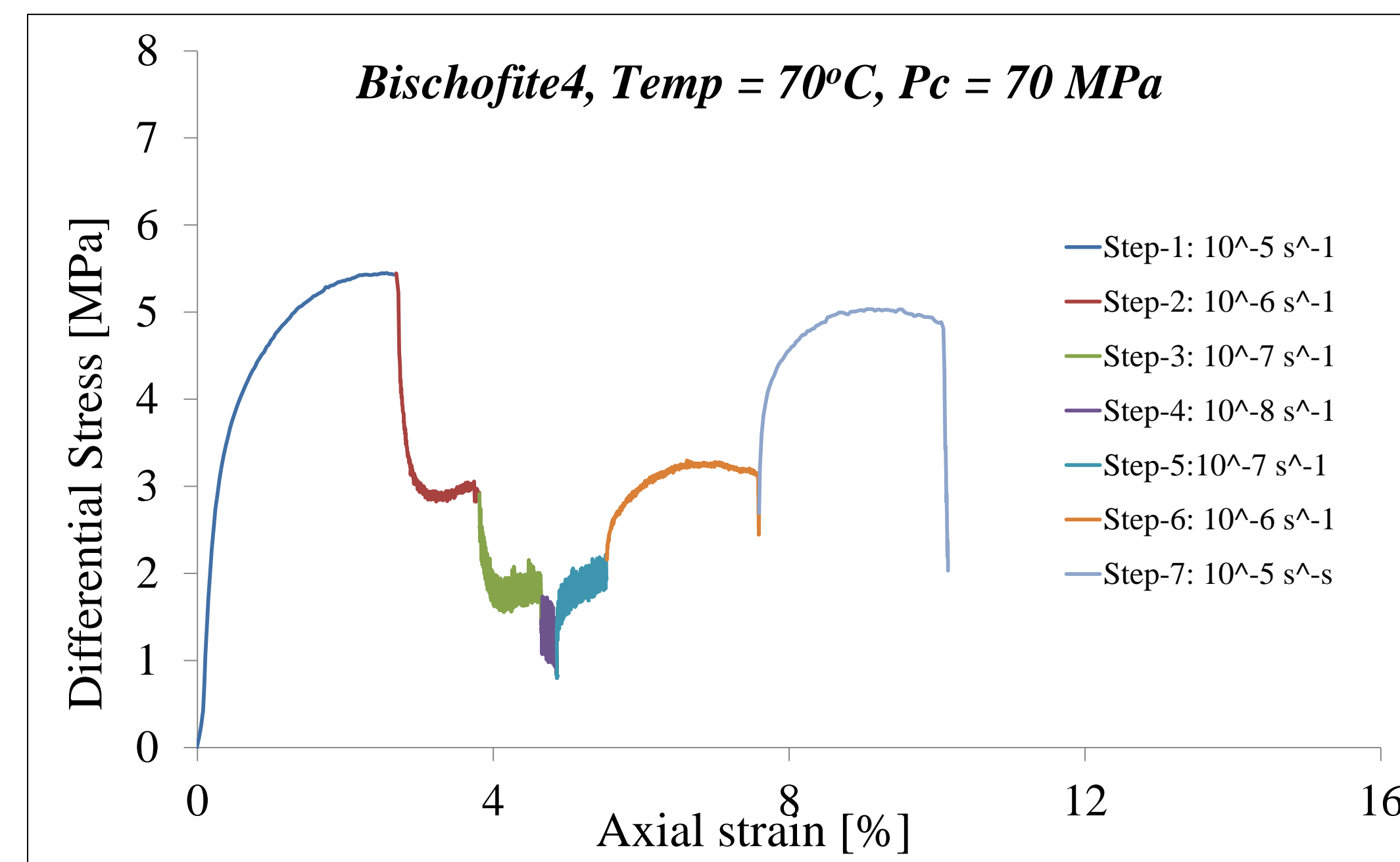


Figure 5. Strain rate sensitivity of flow stress at 70 MPa

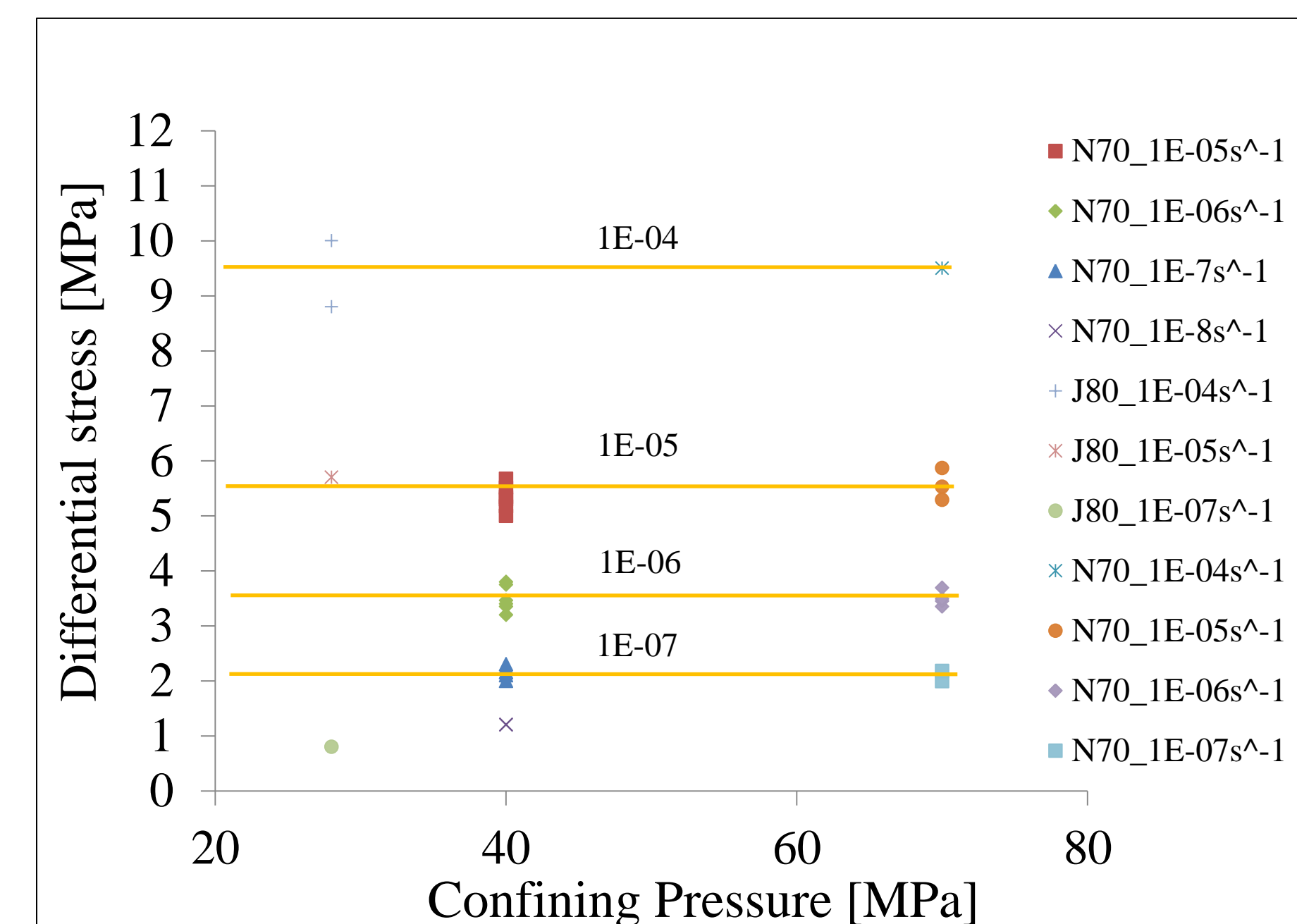


Figure 6. No Effect of confining pressure

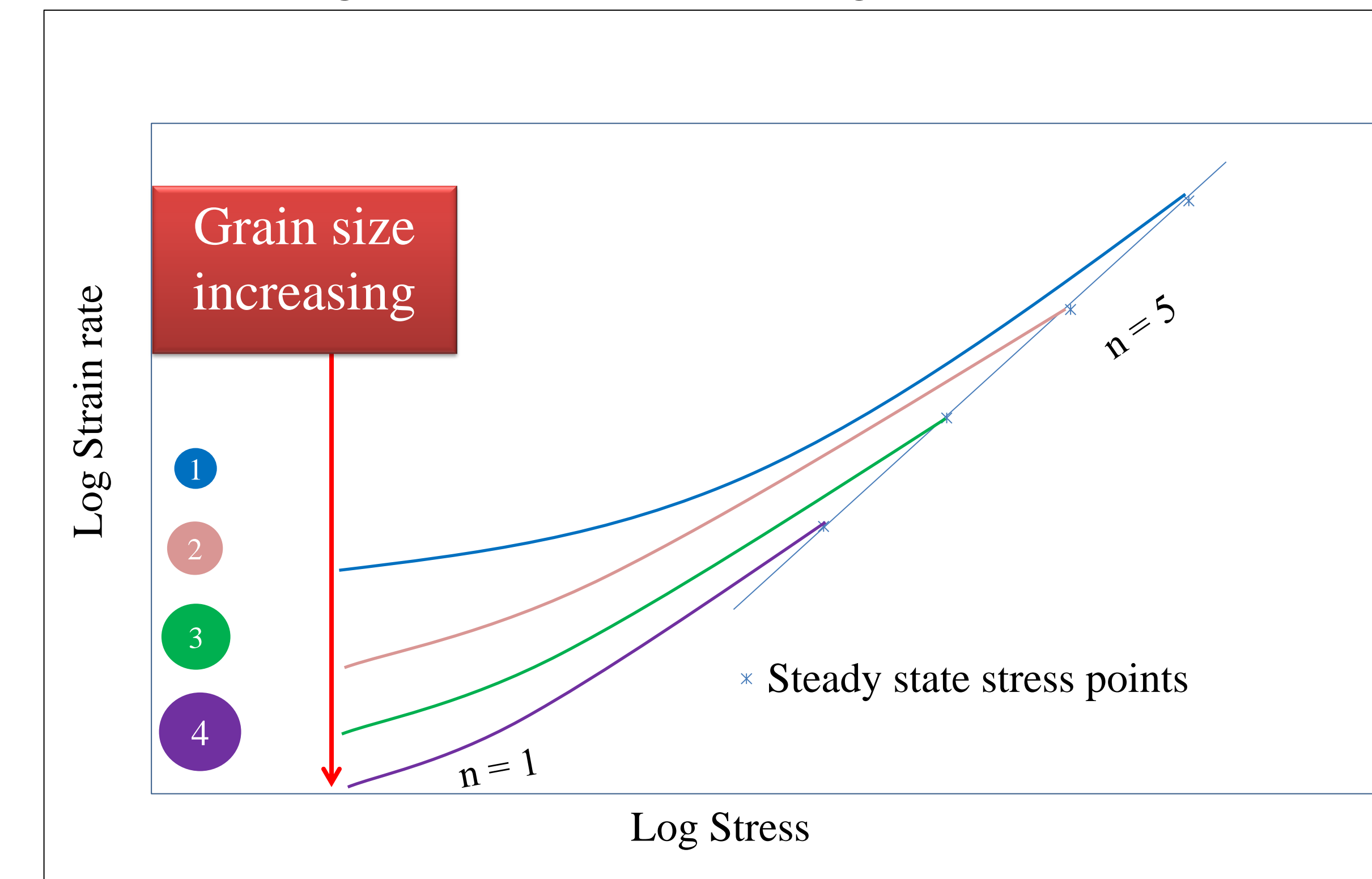


Figure 11. Schematic diagram: Changing n-value during relaxation

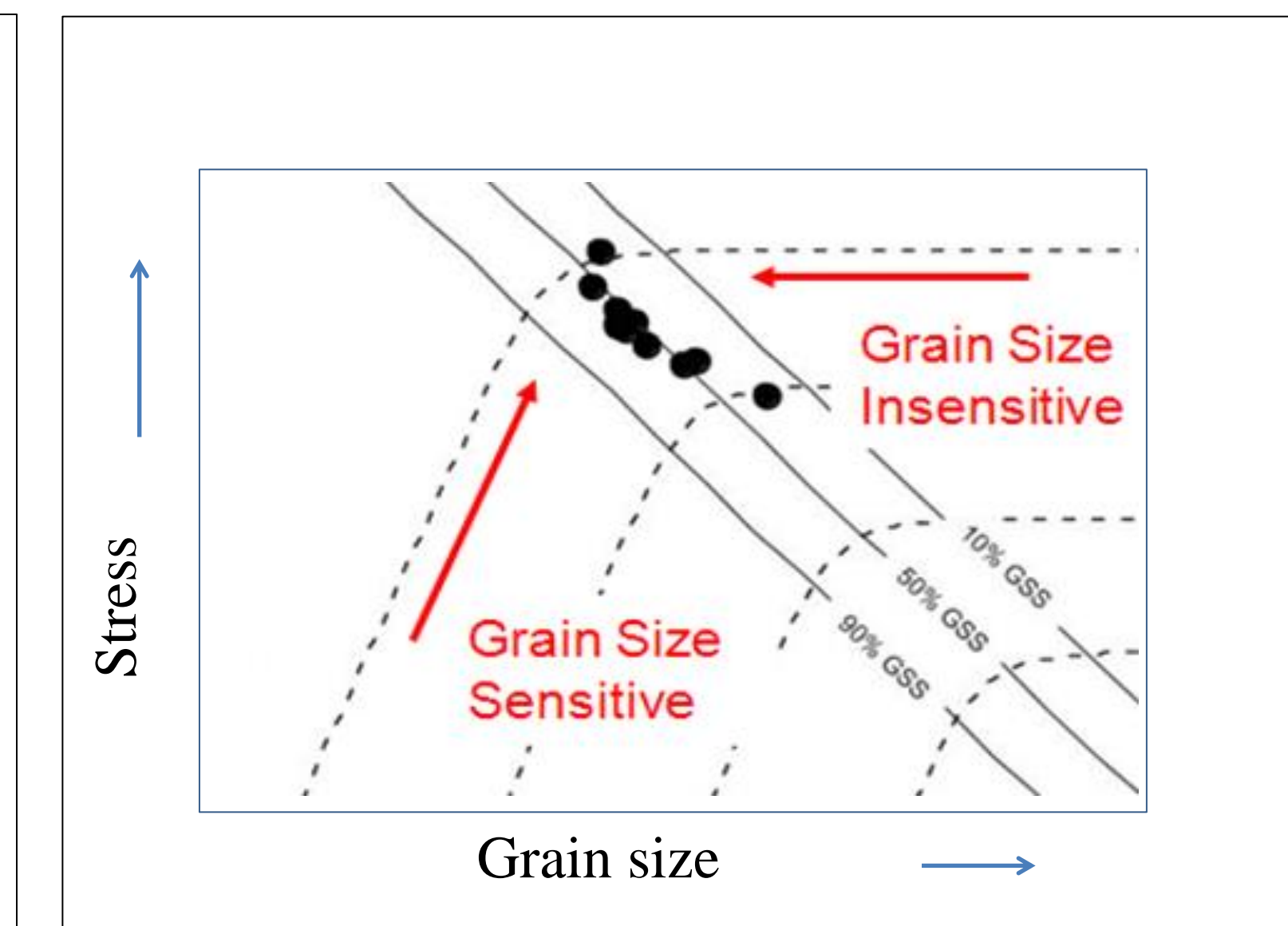


Figure 12. Boundary hypothesis

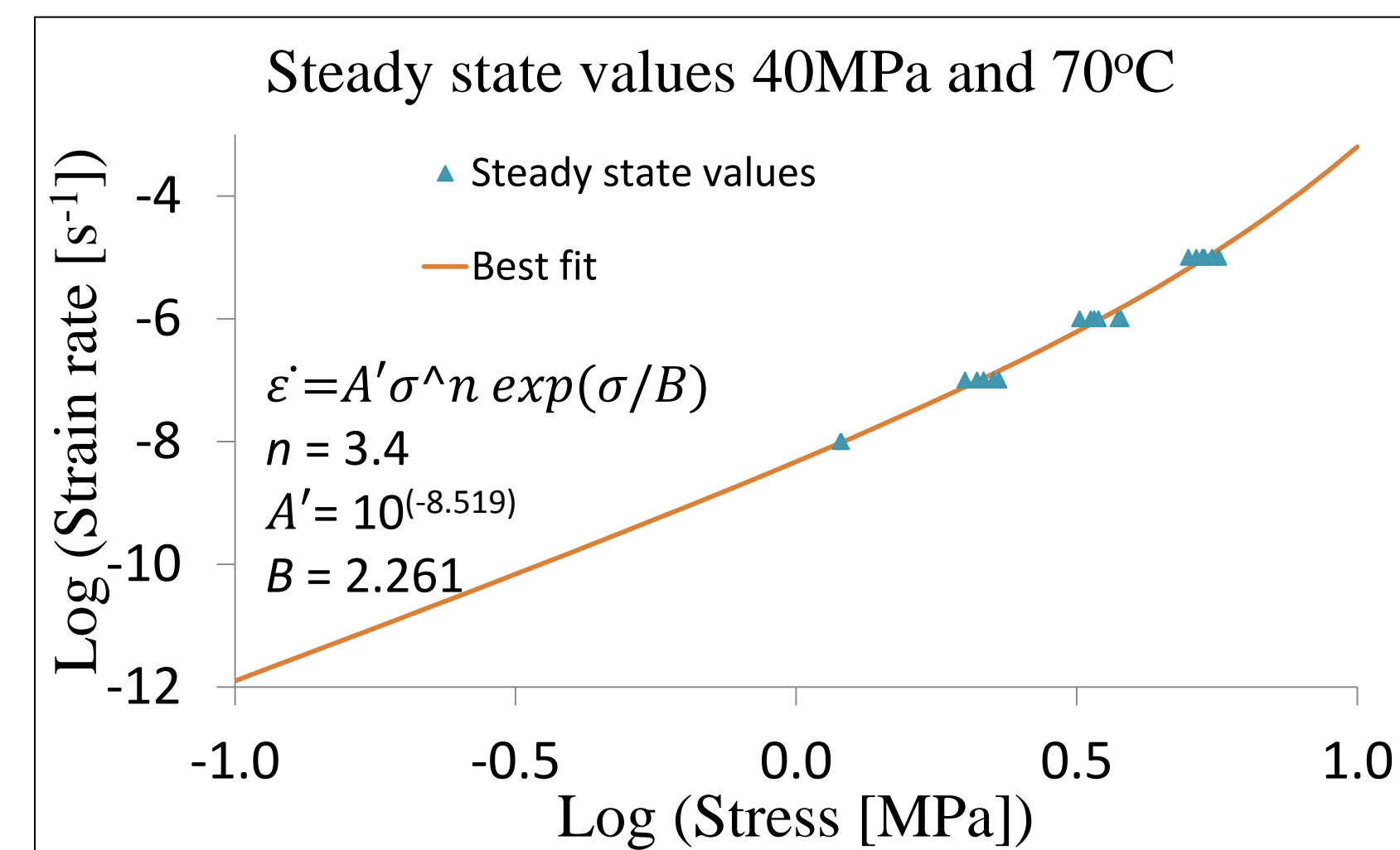


Figure 7. Non-linear trend of steady state points

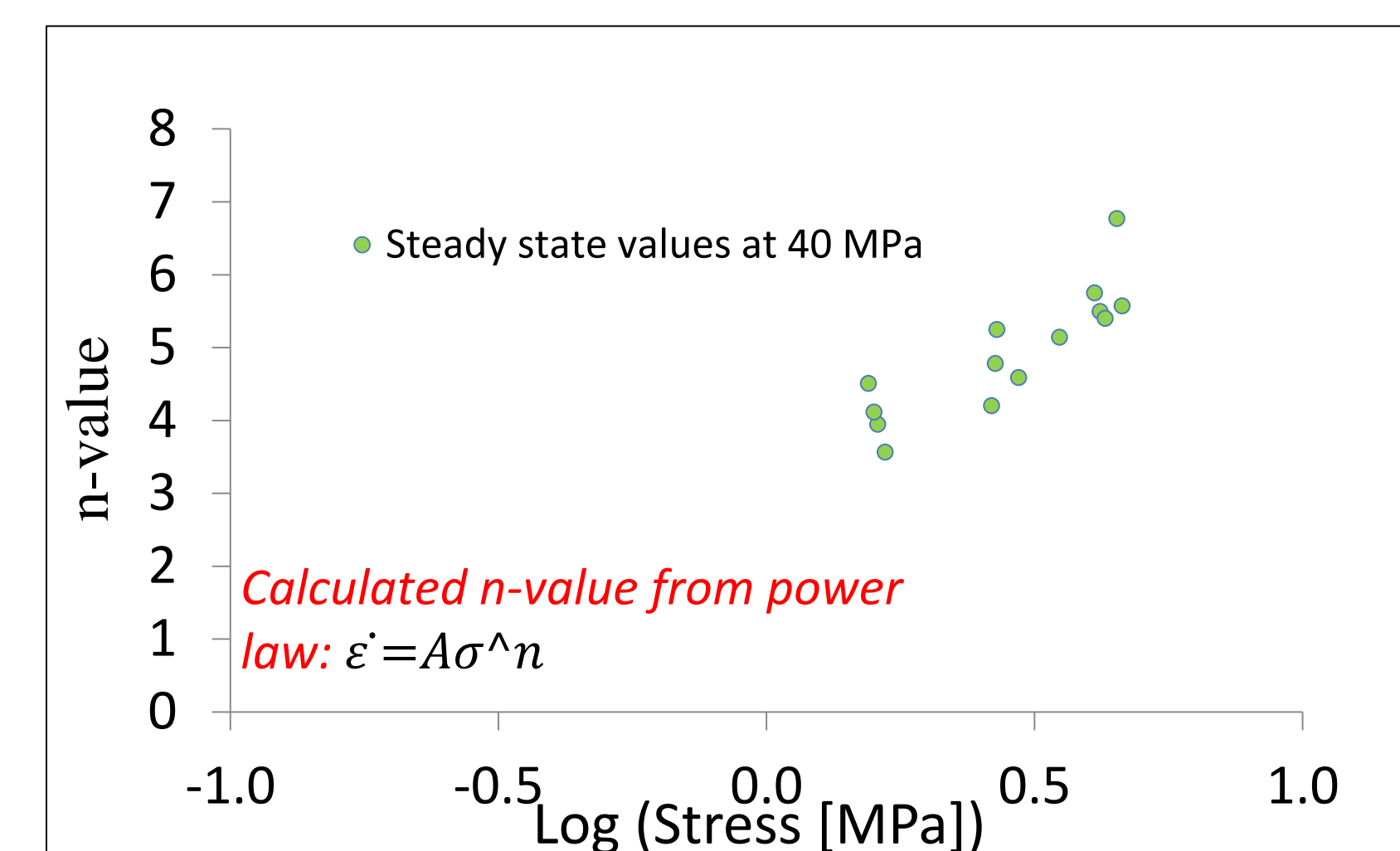


Figure 8. n-value vs. log of steady state stress

### 3. Mechanical behaviour:

- Strength of bischofite is strain rate sensitive.
- Steady state stress values are reasonably well reproducible
- Steady state stress values do not follow linear trend on  $\log \sigma - \log \dot{\epsilon}$  plot, so conventional power law cannot be used.
- No pressure sensitivity of strength at tested conditions.
- Bischofite is weaker during relaxation than during deformation at constant strain rate, at the same stress.

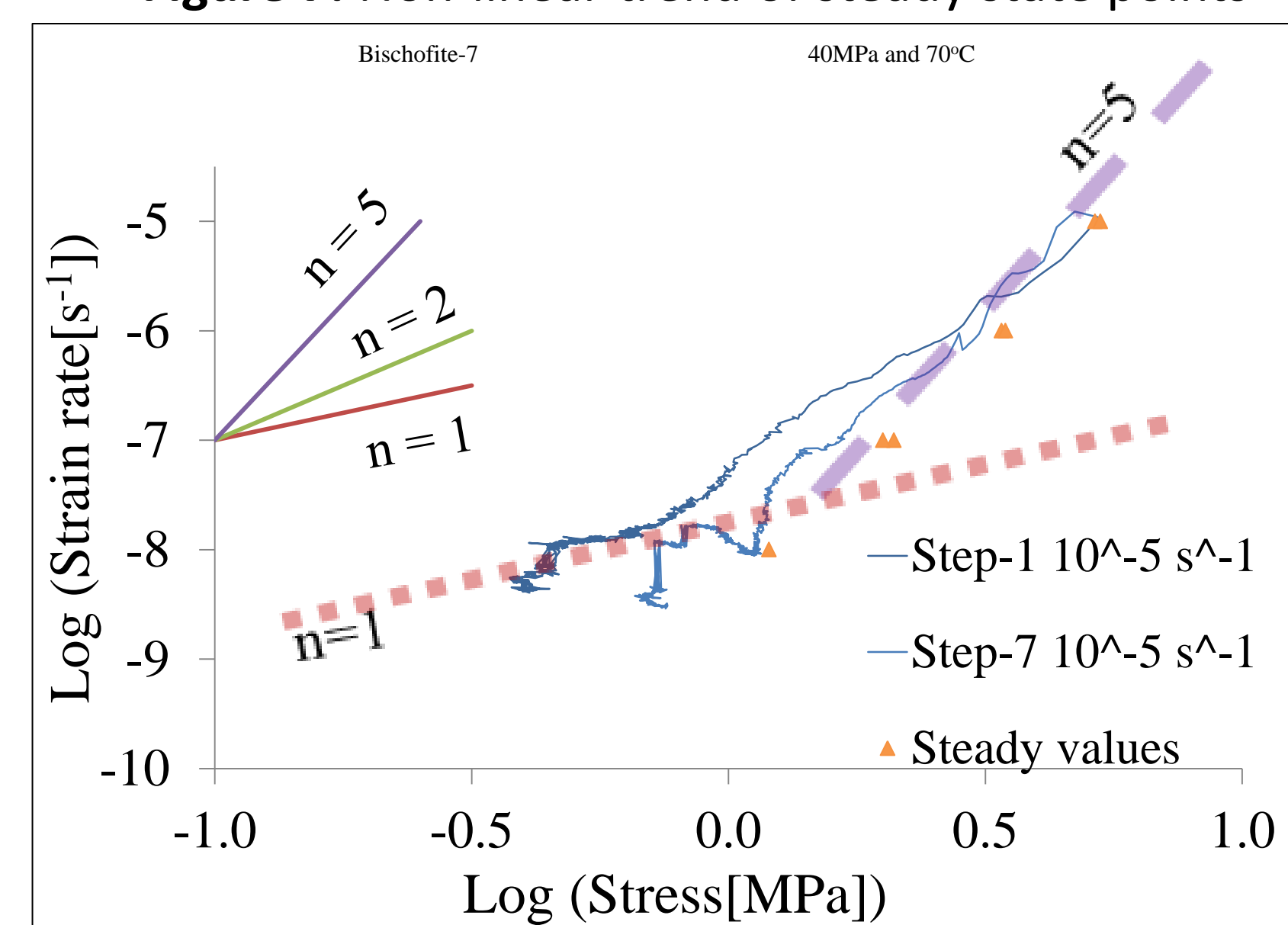
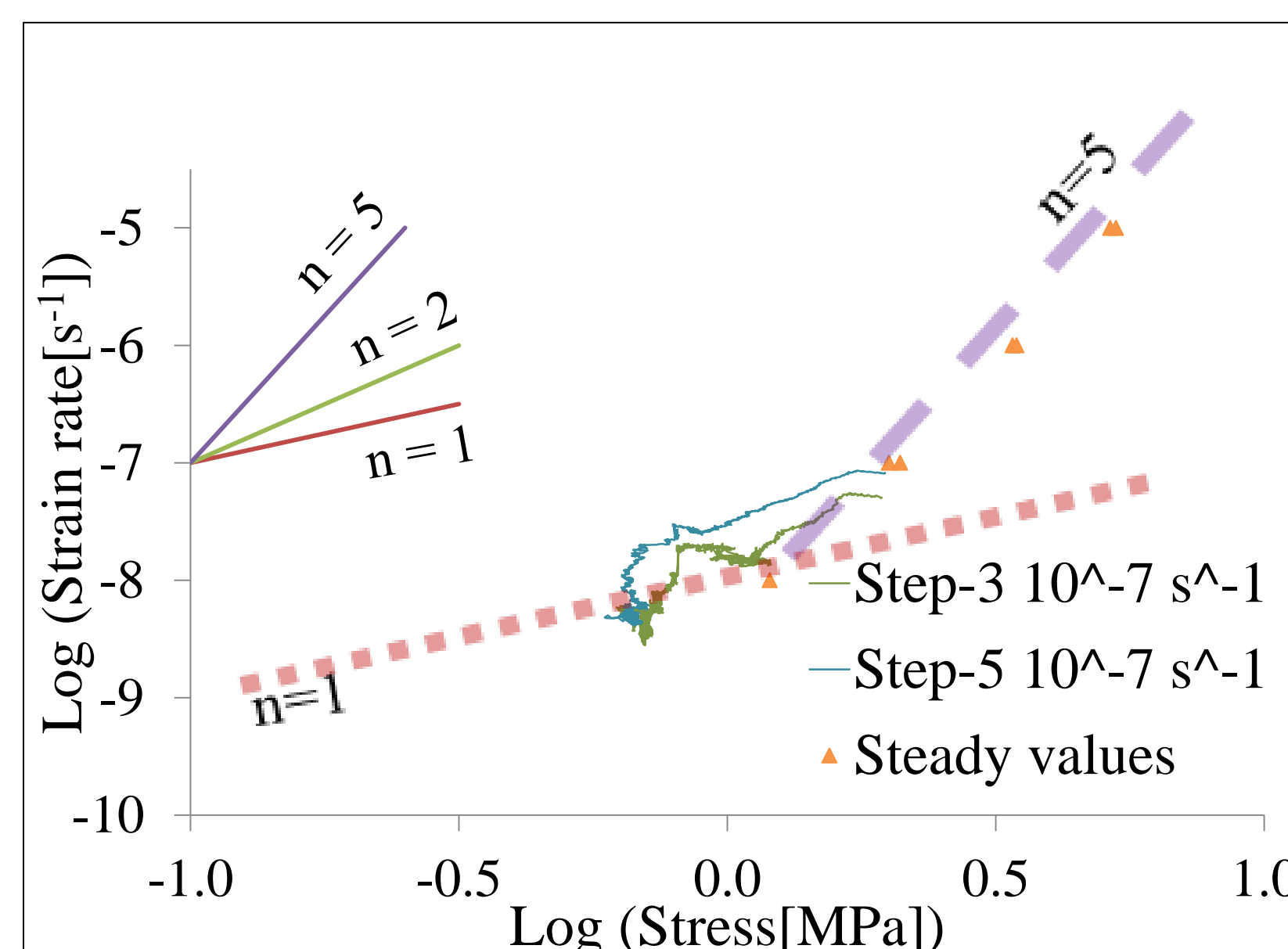
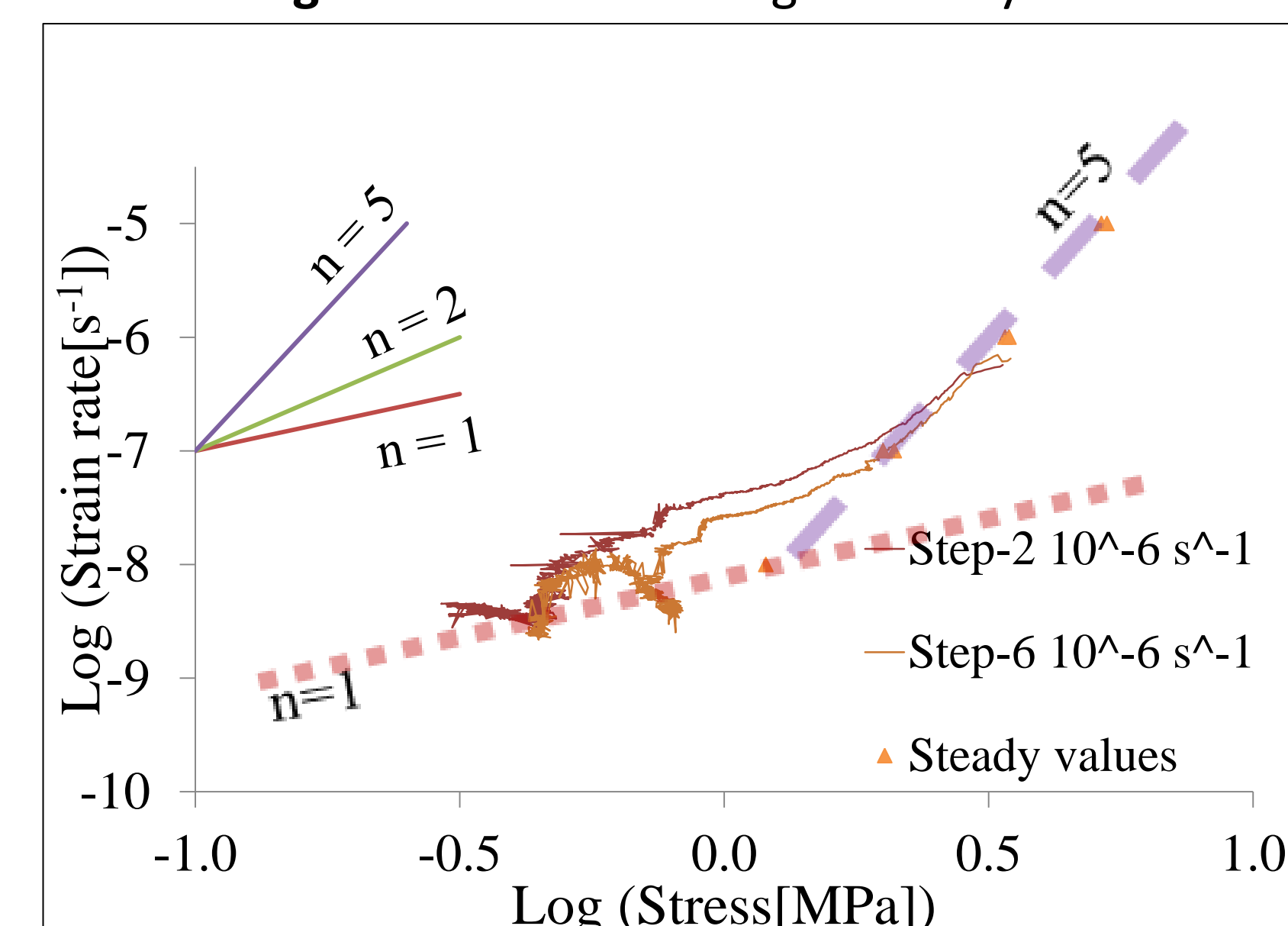


Figure 9. Stress relaxation curves with steady state differential stress values. Similar strain rate steps are combined to see the reproducibility.



### 6. Conclusions:

- Observed behaviour differs between constant strain rate steps and relaxation periods.
- Trend to  $n = 1$ , in relaxation not seen at constant strain rate.
- Implies effective microstructural modification
- So balance between GSI and GSS? of "boundary hypothesis"
- $\dot{\epsilon}_{total} = \dot{\epsilon}_{GSI} + \dot{\epsilon}_{GSS}$  and  $\dot{\epsilon}_{GSI} \approx \dot{\epsilon}_{GSS} : \dot{\epsilon}_{total} = 2\dot{\epsilon}_{GSI}$
- We propose that a flow law of the type  $\dot{\epsilon} = A'\sigma^n \exp\left(\frac{\sigma}{B}\right)$  should be applied at  $70^\circ\text{C}$  and  $40 \text{ MPa}$ . Best fit analysis resulted in values  $n = 3.4$ ,  $A' = 10^{-(8.519)}$  and  $B = 2.261$ .

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