

## Flow analysis with cumulants: Direct calculations

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Anisotropic flow measurements in heavy-ion collisions provide important information on the properties of hot and dense matter. These measurements are based on analysis of azimuthal correlations and might be biased by contributions from correlations that are not related to the initial geometry, so-called nonflow. To improve anisotropic flow measurements, advanced methods based on multiparticle correlations (cumulants) have been developed to suppress nonflow contribution. These multiparticle correlations can be calculated by looping over all possible multiplets, however, this quickly becomes prohibitively CPU intensive. Therefore, the most used technique for cumulant calculations is based on generating functions. This method involves approximations, and has its own biases, which complicates the interpretation of the results. In this paper we present a new exact method for direct calculations of multiparticle cumulants using moments of the flow vectors.

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### I. INTRODUCTION

Anisotropic flow is a response of the system created in a heavy-ion collision to the anisotropies in the initial geometry. Thus, anisotropic flow is very sensitive to the properties of the system at an early time of its evolution. The sizable azimuthal momentum-space anisotropy observed at relativistic heavy-ion collider (RHIC) energies (for a review, see Refs. [1] and [2]) is the main evidence for the nearly perfect liquid behavior [3,4] of the created matter. Quantitatively, anisotropic flow is characterized by coefficients in the Fourier expansion of the azimuthal dependence of the invariant yield of particles relative to the reaction plane [5,6]:

$$E \frac{d^3 N}{d^3 p} = \frac{1}{2\pi} \frac{d^2 N}{p_t dp_t dy} \left( 1 + \sum_{n=1}^{\infty} 2v_n \cos[n(\phi - \Psi_R)] \right). \quad (1)$$

Here  $E$  is the energy of particle,  $p_t$  is the transverse momentum,  $\phi$  is its azimuthal angle,  $y$  is the rapidity, and  $\Psi_R$  the reaction plane angle (see Fig. 1). The first coefficient,  $v_1$ , is usually called *directed flow*, and the second coefficient,  $v_2$ , is called *elliptic flow*. In general, the  $v_n = \langle \cos[n(\phi - \Psi_{RP})] \rangle$  coefficients are  $p_t$  and  $y$  dependent—in this context we refer to them as *differential flow*. The *integrated flow* is defined as a weighted average with the invariant distribution used as a weight:

$$v_n \equiv \frac{\int_0^\infty v_n(p_t) \frac{dN}{dp_t} dp_t}{\int_0^\infty \frac{dN}{dp_t} dp_t}. \quad (2)$$

Since the reaction plane  $\Psi_R$  is not known experimentally, the anisotropic flow is estimated using azimuthal correlations between the observed particles. For example, using two-particle azimuthal correlations,

$$\langle \cos[n(\phi_1 - \phi_2)] \rangle = \langle e^{in(\phi_1 - \phi_2)} \rangle = \langle v_n^2 \rangle + \delta_n, \quad (3)$$

where the first term,  $\langle v_n^2 \rangle$ , is the part due to anisotropic flow, and  $\delta_n$  represents the so-called nonflow contribution that comes

from correlations not related to the initial system geometry. If nonflow is small, Eq. (3) can be used to measure  $v_n$ , but in general the nonflow contribution is not negligible. To suppress nonflow one can exploit the collective nature of anisotropic flow using multiparticle correlations. The method based on multiparticle cumulants (*genuine* multiparticle correlations) to measure anisotropic flow was proposed in Refs. [7–10]. This method allows to subtract nonflow effects from flow measurements order by order. Note that some experimental artifacts, such as track splitting, in the analysis also contribute to the two-particle correlation; in this respect multiparticle techniques are also valuable, as they suppress such contributions as well.

One of the problems in using multiparticle correlations is the computing power needed to go over all possible particle multiplets, which practically prohibits calculations of correlations of order larger than  $k = 3$  (three-particle correlations). To avoid this problem, it was suggested in Ref. [7] to express cumulants in terms of moments of the magnitude of the corresponding flow vector  $Q_n$ , defined as

$$Q_n \equiv \sum_{i=1}^M e^{in\phi_i}, \quad (4)$$

where  $M$  is the number of particles. Unfortunately, flow estimates from cumulants constructed in such a way were systematically biased by the interference between various harmonics. An improved cumulant method using the formalism of generating functions suggested in Refs. [8] and [9] fixed the problem of interfering harmonics while keeping the number of operations still linear with multiplicity  $M$ . For this approach the analytical calculations become rather tedious and therefore the solutions are obtained using interpolation formulas. Unfortunately this introduces numerical uncertainties and requires tuning of interpolating parameters for different values of the flow harmonics  $v_n$  and multiplicity. More recently a Lee-Yang Zero method (sum generating function) [11–14] has been developed to suppress nonflow contribution to all orders. Closely related to that are methods of Fourier and Bessel transforms of the  $Q$  distributions [15],

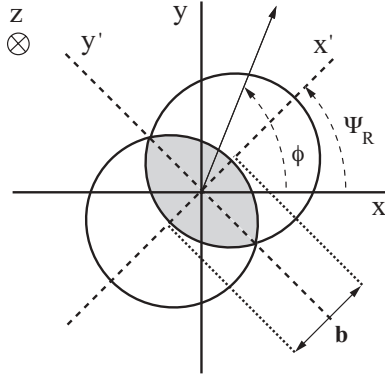


FIG. 1. Schematic view of a noncentral nucleus-nucleus collision in the transverse plane.

and the method of direct fitting of the  $Q$  distribution. All these methods, while indeed being almost insensitive to nonflow, are biased by interference of different harmonics.

In this paper we present a new method to calculate multiparticle cumulants in terms of moments of (in general, different harmonics)  $Q$  vectors. In our approach the cumulants are not biased by interference between various harmonics, interpolating formulas used in the formalism of generating functions are not needed, and, moreover, all detector effects can be disentangled from the flow estimates in a single pass over the data at the level of or better than any other method. The number of operations required in our approach is still  $\propto M$  for each  $k$ . Since in our approach cumulants are calculated without any approximation and directly from the data we often call them *direct cumulants* (also referred to as  $Q$  cumulants because they are expressed analytically in terms of different harmonic  $Q$  vectors).

Flow fluctuations are an important part of an anisotropic flow study. It is believed that flow fluctuations are mostly determined by initial geometry fluctuations [16] of the system created in a collision. An important consequence of this is that the anisotropic flow develops relative to the so-called participant plane(s) instead of the reaction plane determined by the direction of the impact parameter [17]. We note that the method to calculate cumulants proposed in this paper is not influenced by how exactly the anisotropic flow is being developed. We have not discussed issues of the cumulant approach in general, such as multiplicity fluctuations, flow fluctuations, and low sensitivity for small flow values, but believe that our method will be helpful in investigating all these questions.

In our simulations we show results obtained up to the eighth-order cumulant, although we think that in practice there is little advantage to go higher than order six, because going to higher order does not remove the systematic uncertainty related to contribution from clusters exhibiting flow (see the discussion of systematic uncertainties associated with cumulant analysis in Ref. [18]). For example, in a four-particle correlation analysis this bias corresponds to the situation when two particles are correlated because they are coming from the same cluster and, in addition, correlated with another two particles via flow.

The paper is organized as follows. After the main definitions are introduced in Sec. II, we describe how the so-called *reference flow* can be calculated. The reference flow is an average flow in some momentum window; it is needed for the calculation of the differential flow of particles of interest. To optimize the procedure, the reference flow can be calculated using weights, e.g., weighted with transverse momentum of the particle. Thus the reference flow can be noticeably different from integrated flow of the same particles. Section IV describes how the differential flow is calculated. To show how the method works in different environments and how it compares to some other methods we show simulation results in Sec. V. Finally, we summarize the main features of the method. Technical details, including the derivation of the main equations, equations in case of using nonunity weights in the calculation of reference flow, and acceptance effects are provided in Appendices.

## II. MULTIPARTICLE AZIMUTHAL CORRELATIONS AND CUMULANTS

In this paper we discuss mostly two- and four-particle azimuthal correlations (formulas for six-particle correlation are provided in the Appendices), but the generalization to azimuthal correlations involving more particles is straightforward. The method can be easily applied for calculations of *mixed harmonics* multiparticle correlations. In fact, mixed harmonics correlations are needed in our approach for calculations of any multiparticle correlations with order higher than 2. Presenting four-particle correlations below, we also show how the three-particle correlations, involving one particle of a double harmonic, can be calculated. All the correlations are obtained by first averaging over all particles in a given event and then averaging over all events. The latter may involve weights depending on event multiplicity.

We define *single-event* average two- and four-particle azimuthal correlations in the following way:

$$\langle 2 \rangle \equiv \langle e^{in(\phi_1 - \phi_2)} \rangle \equiv \frac{1}{P_{M,2}} \sum'_{i,j} e^{in(\phi_i - \phi_j)}, \quad (5)$$

$$\begin{aligned} \langle 4 \rangle &\equiv \langle e^{in(\phi_1 + \phi_2 - \phi_3 - \phi_4)} \rangle \\ &\equiv \frac{1}{P_{M,4}} \sum'_{i,j,k,l} e^{in(\phi_i + \phi_j - \phi_k - \phi_l)}, \end{aligned} \quad (6)$$

where  $P_{n,m} = n!/(n-m)!$ , and the prime in the sum  $\Sigma'$  means that all indices in the sum must be taken different.

The second step involves averaging over all events:

$$\begin{aligned} \langle \langle 2 \rangle \rangle &\equiv \langle \langle e^{in(\phi_1 - \phi_2)} \rangle \rangle \\ &\equiv \frac{\sum_{\text{events}} (W_{(2)})_i \langle 2 \rangle_i}{\sum_{\text{events}} (W_{(2)})_i}, \end{aligned} \quad (7)$$

$$\begin{aligned} \langle \langle 4 \rangle \rangle &\equiv \langle \langle e^{in(\phi_1 + \phi_2 - \phi_3 - \phi_4)} \rangle \rangle \\ &\equiv \frac{\sum_{\text{events}} (W_{(4)})_i \langle 4 \rangle_i}{\sum_{\text{events}} (W_{(4)})_i}, \end{aligned} \quad (8)$$

where by double brackets we denote an average, first over all particles and then over all events.  $W_{(2)}$  and  $W_{(4)}$  are the event

weights, which are used to minimize the effect of multiplicity variations in the event sample on the estimates of two- and four-particle correlations. In general, the optimal choice of weights would be determined by the multiplicity dependence of  $v_n$ . The best approach might be to calculate the cumulants at fixed  $M$  and then average over the entire event sample. In our calculations, with  $v_n$  independent of multiplicity, we use

$$W_{(2)} \equiv M(M-1), \quad (9)$$

$$W_{(4)} \equiv M(M-1)(M-2)(M-3). \quad (10)$$

The above choice for the event weights takes into account the number of different two- and four-particle combinations in an event with multiplicity  $M$ .

The general formalism of cumulants was introduced for flow analysis by Ollitrault *et al.* [7–9]. We will use below the notations from those papers. The second-order cumulant,  $c_n\{2\}$ , is simply an average of two-particle correlation defined in Eq. (7):

$$c_n\{2\} = \langle\langle 2 \rangle\rangle. \quad (11)$$

As was pointed out first in Ref. [8], the *genuine* four-particle correlation (i.e., four-particle cumulant) is given by

$$c_n\{4\} = \langle\langle 4 \rangle\rangle - 2 \cdot \langle\langle 2 \rangle\rangle^2. \quad (12)$$

Expressions (11) and (12) are applicable only for detectors with uniform acceptance and will be generalized in Appendix C to extend their applicability for detectors with nonuniform acceptance.

Different order cumulants provide independent estimates for the same reference harmonic  $v_n$ . In particular [8],

$$v_n\{2\} = \sqrt{c_n\{2\}}, \quad (13)$$

$$v_n\{4\} = \sqrt[4]{-c_n\{4\}}, \quad (14)$$

where the notation  $v_n\{2\}$  is used to denote the reference flow  $v_n$  estimated from the second-order cumulant  $c_n\{2\}$ , and  $v_n\{4\}$  stands for the reference flow  $v_n$  estimated from the fourth-order cumulant  $c_n\{4\}$ .

### III. REFERENCE FLOW

To obtain the second-order cumulant it suffices to separate diagonal and off-diagonal terms in  $|Q_n|^2$ :

$$|Q_n|^2 = \sum_{i,j=1}^M e^{in(\phi_i-\phi_j)} = M + \sum_{i,j}' e^{in(\phi_i-\phi_j)}, \quad (15)$$

which can be trivially solved to obtain  $\langle 2 \rangle$ :

$$\langle 2 \rangle = \frac{|Q_n|^2 - M}{M(M-1)}. \quad (16)$$

The event averaging is being performed via Eq. (7). The resulting expression for  $\langle\langle 2 \rangle\rangle$  is then used to estimate the second-order cumulant [see Eq. (11)], which in turn is used to estimate the reference flow harmonic  $v_n$  by making use of Eq. (13).

To obtain the fourth-order cumulant we start with identifying the four-particle correlations in the decomposition of  $|Q_n|^4$

(for details, see Appendix A):

$$|Q_n|^4 = Q_n Q_n Q_n^* Q_n^* = \sum_{i,j,k,l=1}^M e^{in(\phi_i+\phi_j-\phi_k-\phi_l)}. \quad (17)$$

This sum contains terms corresponding to four distinct combinations of the indices  $i, j, k$ , and  $l$ : (1) They are all different (four-particle correlation), (2) three are different, (3) two are different, or (4) they are all the same. Explicit expressions for all the terms are given in Eq. (A6). Note that the case of three different indices corresponds to the so-called mixed harmonics three-particle correlations, in many analyses of great interest by themselves [18,19]. Equations for three-particle correlations are provided in Appendix A. Taking everything into account, we obtain the following analytic result for the single-event average four-particle correlation defined in Eq. (6):

$$\langle 4 \rangle = \frac{|Q_n|^4 + |Q_{2n}|^2 - 2 \cdot \text{Re}[Q_{2n} Q_n^* Q_n^*]}{M(M-1)(M-2)(M-3)} - 2 \frac{2(M-2) \cdot |Q_n|^2 - M(M-3)}{M(M-1)(M-2)(M-3)}. \quad (18)$$

The reason why the originally proposed cumulant analysis [7] was biased lies in the fact that the terms consisting of  $Q$  vectors evaluated in *different* harmonics (for instance, terms  $|Q_{2n}|^2$  and  $\text{Re}[Q_{2n} Q_n^* Q_n^*]$ ) have been neglected. As seen from Eq. (18), such terms do appear in the analytic results and are crucial in disentangling the interference between harmonics. In particular, if a higher harmonic  $v_{2n}$  is present, then  $|Q_n|^4$  picks up an additional contribution depending on that harmonic, namely,  $v_{2n}^2 M(M-1) + v_n^2 v_{2n} 2M(M-1)(M-2)$ , which is exactly canceled out with the contribution of harmonic  $v_{2n}$  to  $|Q_{2n}|^2$  and  $\text{Re}[Q_{2n} Q_n^* Q_n^*]$ , which read  $M v_{2n}^2 (M-1)$  and  $M(M-1)(M-2) v_n^2 v_{2n} + M(M-1) v_{2n}^2$ , respectively.

The final, event-averaged four-particle azimuthal correlation,  $\langle\langle 4 \rangle\rangle$ , is then obtained by making use of Eqs. (8) and (10). Using  $\langle\langle 4 \rangle\rangle$  and  $\langle\langle 2 \rangle\rangle$  one can calculate the fourth-order cumulant from Eq. (12).

The reference flow is mainly used to calculate differential flow. Therefore, one can optimize the calculation of reference flow to minimize the uncertainties in the final results. This is done by using different weights (e.g., particle transverse momentum) in the definition of flow vectors used in reference flow calculations. We provide all the equations necessary for calculations with weights in Appendix B.

The equations so far are applicable for an analysis with a detector with full uniform azimuthal coverage. In a nonideal case one needs to take into account the acceptance corrections [12,20]. Acceptance affects the cumulants in three ways: (i) contributions from additional terms, e.g., proportional to  $\langle\langle \cos n\phi \rangle\rangle$  or  $\langle\langle \sin n\phi \rangle\rangle$ , that for a detector with full uniform azimuthal coverage are identical to zero, (ii) contributions from other flow harmonics, and (iii) the cumulant might be rescaled, which at the end can affect the final extracted flow values. We refer to Refs. [12] and [20] for a more complete discussion of acceptance effects. In practice, the most important correction is the first one, for which we provide the full set of equations for a two- and four-particle cumulant analysis.

The generalized second-order cumulant which can also be used for detectors with nonuniform acceptance is

$$\begin{aligned} c_n\{2\} &= \langle\langle 2 \rangle\rangle - \text{Re}\{\langle\langle \cos n\phi_1 \rangle\rangle + i\langle\langle \sin n\phi_1 \rangle\rangle\} \\ &\quad \times [\langle\langle \cos n\phi_2 \rangle\rangle - i\langle\langle \sin n\phi_2 \rangle\rangle] \\ &= \langle\langle 2 \rangle\rangle - \langle\langle \cos n\phi_1 \rangle\rangle^2 - \langle\langle \sin n\phi_1 \rangle\rangle^2, \end{aligned} \quad (19)$$

where for the last line we have used the fact that, for instance,  $\langle\langle \cos n\phi_1 \rangle\rangle$  and  $\langle\langle \cos n\phi_2 \rangle\rangle$  are the same quantities apart from the trivial relabeling. Remarkably, only two additional terms appear in Eq. (19), namely,  $\langle\langle \cos n\phi_1 \rangle\rangle^2$  and  $\langle\langle \sin n\phi_1 \rangle\rangle^2$ , which counterbalance the bias to  $\langle\langle 2 \rangle\rangle$  coming from very general detector inefficiencies. Further details on treating the acceptance effects, including formulas for the fourth-order cumulant are provided in Appendix C.

#### IV. DIFFERENTIAL FLOW

Once the reference flow has been estimated with the help of the formalism from the previous section, we proceed to the calculation of differential flow. For that, all particles selected for flow analysis are labeled as *reference flow particle* (RFP) and/or *particle of interest* (POI). These labels are needed because flow analysis is being performed in two steps. In the first step one estimates the reference flow by using only the RFPs, while in the second step we estimate the differential flow of POIs with respect to the reference flow of the RFPs obtained in the first step.

##### A. Reduced multiparticle azimuthal correlations

For *reduced* single-event average two- and four-particle azimuthal correlations we use the following notations and definitions:

$$\begin{aligned} \langle 2' \rangle &\equiv \langle e^{in(\psi_1 - \phi_2)} \rangle \\ &\equiv \frac{1}{m_p M - m_q} \sum_{i=1}^{m_p} \sum_{j=1}^M ' e^{in(\psi_i - \phi_j)}, \end{aligned} \quad (20)$$

$$\begin{aligned} \langle 4' \rangle &\equiv \langle e^{in(\psi_1 + \phi_2 - \phi_3 - \phi_4)} \rangle \\ &\equiv \frac{1}{(m_p M - 3m_q)(M-1)(M-2)} \\ &\quad \times \sum_{i=1}^{m_p} \sum_{j,k,l=1}^M ' e^{in(\psi_i + \phi_j - \phi_k - \phi_l)}, \end{aligned} \quad (21)$$

where  $m_p$  is the total number of particles labeled as POI (some of which might have been also labeled additionally as RFP),  $m_q$  is the total number of particles labeled *both* as RFP and POI,  $M$  is the total number of particles labeled as RFP (some of which might have been also labeled additionally as POI) in the event,  $\psi_i$  is the azimuthal angle of the  $i$ th particle labeled as POI and taken from the phase window of interest (taken even if it was also additionally labeled as RFP),  $\phi_j$  is the azimuthal angle of the  $j$ th particle labeled as RFP (taken even if it was also additionally labeled as POI).  $\Sigma'$ , as before, denotes the sum with all indices taken different.

Finally, event averaged reduced two- and four-particle correlations are given by

$$\langle\langle 2' \rangle\rangle \equiv \frac{\sum_{\text{events}} (w_{\langle 2' \rangle})_i \langle 2' \rangle_i}{\sum_{\text{events}} (w_{\langle 2' \rangle})_i}, \quad (22)$$

$$\langle\langle 4' \rangle\rangle \equiv \frac{\sum_{\text{events}} (w_{\langle 4' \rangle})_i \langle 4' \rangle_i}{\sum_{\text{events}} (w_{\langle 4' \rangle})_i}. \quad (23)$$

In our calculations we use event weights  $w_{\langle 2' \rangle}$  and  $w_{\langle 4' \rangle}$  defined as

$$w_{\langle 2' \rangle} \equiv m_p M - m_q, \quad (24)$$

$$w_{\langle 4' \rangle} \equiv (m_p M - 3m_q)(M-1)(M-2). \quad (25)$$

##### B. Differential cumulants

We derive equations for the differential cumulants with the help of  $p$  and  $q$  vectors, the former built out of all POIs ( $m_p$  in total), and the second only from POI labeled also as RFP ( $m_q$  in total):

$$p_n \equiv \sum_{i=1}^{m_p} e^{in\psi_i}, \quad (26)$$

$$q_n \equiv \sum_{i=1}^{m_q} e^{in\psi_i}. \quad (27)$$

The  $q$  vector is introduced here in order to subtract effects of autocorrelations. Using the  $p$  and  $q$  vectors, we have obtained the following equations for the average reduced single- and all-event two-particle correlations:

$$\langle 2' \rangle = \frac{p_n Q_n^* - m_q}{m_p M - m_q}, \quad (28)$$

$$\langle\langle 2' \rangle\rangle = \frac{\sum_{i=1}^N (w_{\langle 2' \rangle})_i \langle 2' \rangle_i}{\sum_{i=1}^N (w_{\langle 2' \rangle})_i}. \quad (29)$$

For detectors with uniform azimuthal acceptance the differential second-order cumulant is given by

$$d_n\{2\} = \langle\langle 2' \rangle\rangle, \quad (30)$$

where again we use notation from Ref. [8]. We present equations for the case of detectors with nonuniform acceptance in Appendix C.

Estimates of differential flow  $v'_n$  are being denoted as  $v'_n\{2\}$  and are given by [8]

$$v'_n\{2\} = \frac{d_n\{2\}}{\sqrt{c_n\{2\}}}. \quad (31)$$

Below we present the corresponding formulas for reduced four-particle correlations:

$$\begin{aligned} \langle 4' \rangle &= [p_n Q_n Q_n^* Q_n^* - q_{2n} Q_n^* Q_n^* - p_n Q_n Q_{2n}^* \\ &\quad - 2 \cdot M p_n Q_n^* - 2 \cdot m_q |Q_n|^2 + 7 \cdot q_n Q_n^* \\ &\quad - Q_n q_n^* + q_{2n} Q_{2n}^* + 2 \cdot p_n Q_n^* + 2 \cdot m_q M \\ &\quad - 6 \cdot m_q] / [(m_p M - 3m_q)(M-1)(M-2)], \end{aligned} \quad (32)$$

$$\langle\langle 4' \rangle\rangle = \frac{\sum_{i=1}^N (w_{\langle 4' \rangle})_i \langle 4' \rangle_i}{\sum_{i=1}^N (w_{\langle 4' \rangle})_i}. \quad (33)$$

The fourth-order differential cumulant is given by [8]

$$d_n\{4\} = \langle\langle 4' \rangle\rangle - 2 \cdot \langle\langle 2' \rangle\rangle \langle\langle 2 \rangle\rangle. \quad (34)$$

Equations for the case of detectors with nonuniform acceptance are again presented in Appendix C.

Having obtained estimates for  $d_n\{4\}$  and  $c_n\{4\}$ , we can estimate differential flow [8]:

$$v_n'\{4\} = -\frac{d_n\{4\}}{(-c_n\{4\})^{3/4}}. \quad (35)$$

Similarly to reference flow, we use the notation  $v_n'\{4\}$  for differential flow harmonics  $v_n'$  obtained from fourth-order cumulants.  $v_n'\{4\}$  and  $v_n'\{2\}$  are independent estimates for the same differential flow harmonic  $v_n'$ .

## V. SIMULATION RESULTS

We have tested the new method with extensive simulations. The results, presented below, show that the method effectively suppresses nonflow contributions, illustrate the ability to remove the interference of the different harmonics, show the applicability for detectors having significant acceptance ‘‘holes,’’ and give an example of a differential flow analysis. In the figures,  $v_2\{\text{MC}\}$ , shown in the first bin, represents the Monte Carlo estimate for  $v_n$ , which was obtained using the known reaction plane event by event. Other estimates in the figures are obtained without using this information.

Figure 2 shows the results from a simulation of events with anisotropic flow present in two harmonics, the second and the fourth. Elliptic flow estimated by different methods is shown in the figure. A clear bias is observed in the estimates from fitting of the  $Q$ -distribution method and the Lee-Yang zero method (sum generating function), labeled as  $v_2\{\text{FQD}\}$  and  $v_2\{\text{LYZS}\}$ , respectively. Results obtained with direct cumulants of different order, labeled as  $v_2\{k, \text{QC}\}$ , are unaffected by  $v_4$  interference.

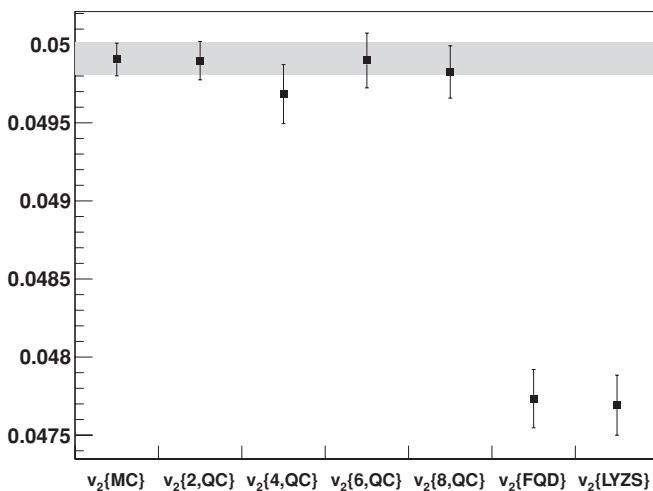
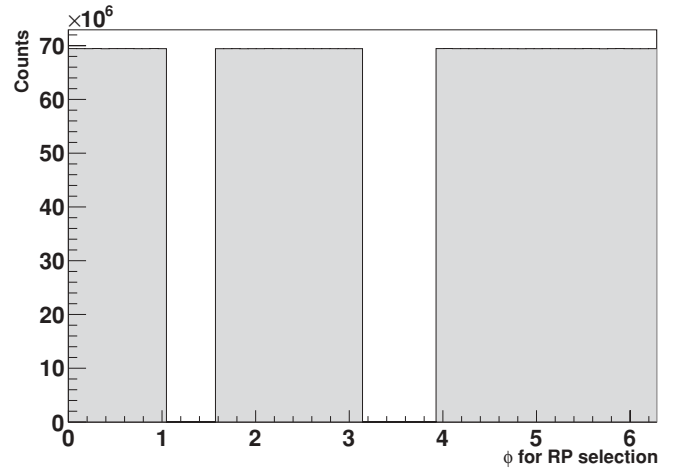
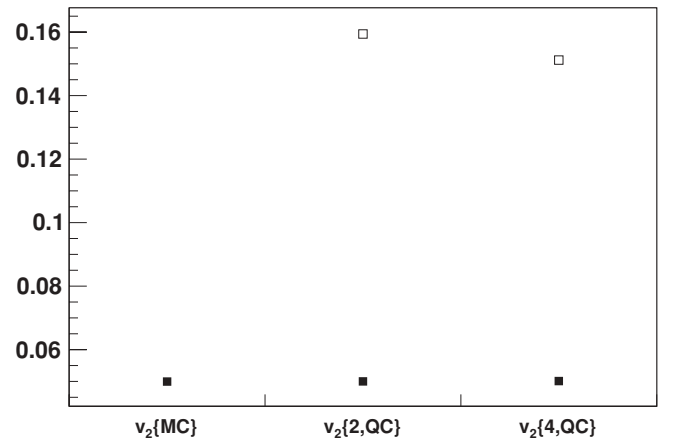


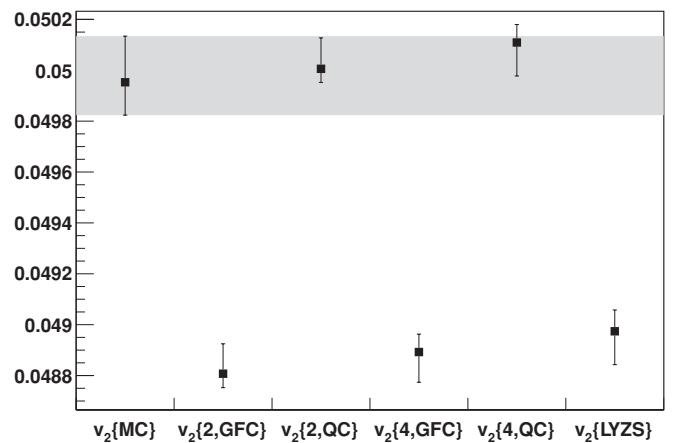
FIG. 2. Elliptic flow extracted by different methods for  $10^5$  simulated events with multiplicity  $M = 500$ ,  $v_2 = 0.05$ , and at the same time  $v_4 = 0.1$ . MC denotes the Monte Carlo estimate for  $v_2$ , QC stands for  $Q$ -cumulant estimates, FQD denotes estimate obtained from fitting  $Q$  distribution, and finally LYZS marks the estimate from the Lee-Yang zero method (sum generating function).



(a)



(b)



(c)

FIG. 3. (a) The azimuthal distribution of accepted particles. (b) Extracted elliptic flow accounting for acceptance effects, closed markers, and without open markers. (c) Extracted elliptic flow accounting for acceptance effects in different methods.

To demonstrate that the method works well even in cases with rather bad acceptance, we simulated  $10^7$  events with  $v_2 = 0.05$  for a detector that had two large ‘‘holes’’ [see Fig. 3(a)].

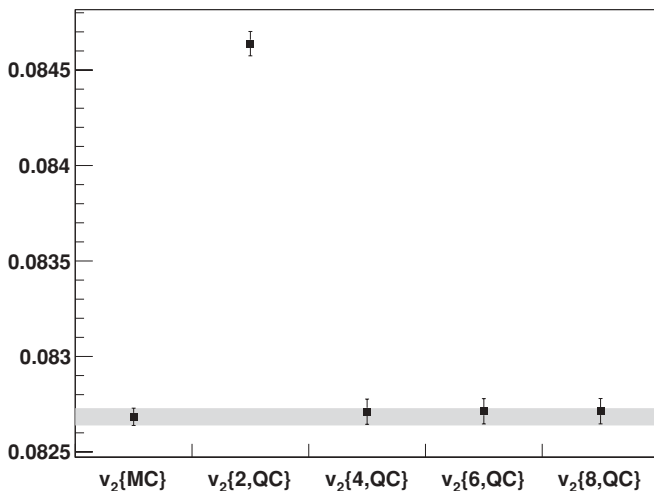


FIG. 4. Reference flow extracted from particles labeled as RFPs (pions in Therminator).

Figure 3(b) shows the obtained  $v_2$  estimates using Eqs. (11) and (12), which are valid for detectors with perfect acceptance using open markers. Clearly these values are strongly biased. The  $v_2$  estimates obtained from the more general equations for cumulants, namely, Eqs. (C1) and (C6), which do account for the acceptance effects are shown as closed markers and agree with the Monte Carlo estimate. In Fig. 3(c) we look in more detail at the agreement with the Monte Carlo estimate and, in addition, compare to other methods. The figure clearly shows that detector effects are corrected for at the level of or better than other methods.

As an example of a differential flow analysis we show results for  $v_2'(p_t)$  obtained with Therminator [21]. As RFPs we select pions and as POIs we select protons. In the first step we estimate the reference flow by only making use of particles labeled as RFPs [using Eqs. (11)–(14)]. The estimates

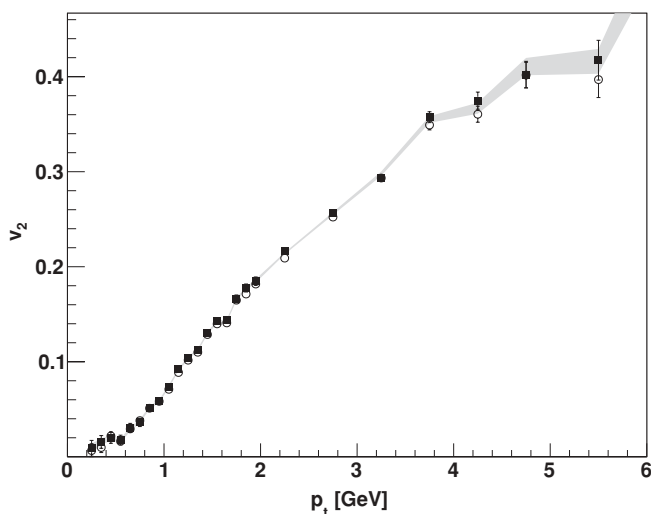


FIG. 5. Differential flow extracted for particles labeled as POIs from Therminator events (in this example we used protons). The open circles denote a second-order estimate [Eq. (31)] and closed squares denote a fourth-order estimate [Eq. (35)].

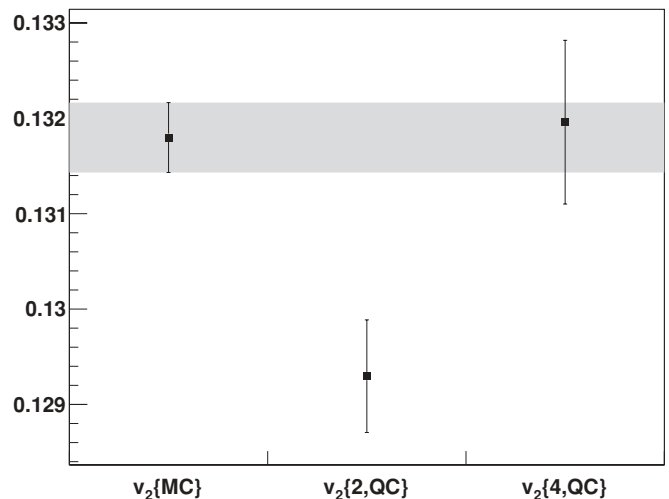


FIG. 6.  $p_t$ -integrated flow calculated from Eq. (2) of protons whose differential flow is presented in Fig. 5.

of reference flow are presented in Fig. 4. In the second step we estimate the differential flow of POIs (in this example protons were labeled as POIs) with respect to the reference flow of RFPs estimated in the first step. For each  $p_t$  bin we evaluate  $d_n\{2\}$  and  $d_n\{4\}$ , and use Eqs. (31) and (35) to estimate differential flow. The differential flow results for protons are presented in Fig. 5. The resulting  $p_t$ -integrated flow of protons calculated by making use of Eq. (2) is presented in Fig. 6. The figures for the integrated flow of the RFPs and POIs clearly show that the second-order cumulant is biased by nonflow while the higher-order cumulants are in perfect agreement with the Monte Carlo.

## VI. SUMMARY

In summary, we propose a new method to calculate multiparticle azimuthal correlations, which provides fast (in a single scan over the data) and exact (no approximations) nonbiased (no interference between different harmonics) estimates for cumulants. In the paper, we provide the corresponding formulas for correlations up to the sixth order, but the method, if needed, can be generalized for higher orders.

The proposed method has been extensively tested in simulations and has been used for real data analysis by the STAR and ALICE Collaborations [22–24]. Further details about the method, including equations for eight-particle correlations, equations for estimates and evaluation of statistical errors, and comparison to other methods can be found in Ref. [23].

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### APPENDIX A: EQUATIONS FOR THREE-, FOUR-, AND SIX-PARTICLE CORRELATIONS

Below we use the following definitions:

$$\langle 2 \rangle \equiv \langle 2 \rangle_{n|n} \equiv \frac{1}{P_{M,2}} \sum_{i,j=1}^M e^{in(\phi_i - \phi_j)}, \quad (\text{A1})$$

$$\langle 2 \rangle_{2n|2n} \equiv \frac{1}{P_{M,2}} \sum_{i,j=1}^M e^{i2n(\phi_i - \phi_j)}, \quad (\text{A2})$$

$$\langle 3 \rangle_{2n|n,n} \equiv \frac{1}{P_{M,3}} \sum_{i,j,k=1}^M e^{in(2\phi_i - \phi_j - \phi_k)}, \quad (\text{A3})$$

$$\langle 3 \rangle_{n,n|2n} \equiv \langle 3 \rangle_{2n|n,n}^*, \quad (\text{A4})$$

$$\langle 4 \rangle \equiv \langle 4 \rangle_{n,n|n,n} \equiv \frac{1}{P_{M,4}} \sum_{i,j,k,l=1}^M e^{in(\phi_i + \phi_j - \phi_k - \phi_l)}. \quad (\text{A5})$$

Using this notation one finds

$$\begin{aligned} |Q_n|^4 &= \langle 4 \rangle_{n,n|n,n} \cdot P_{M,4} + [\langle 3 \rangle_{2n|n,n} + \langle 3 \rangle_{n,n|2n}] \cdot P_{M,3} \\ &+ \langle 2 \rangle_{n|n} \cdot 4P_{M,2}(M-1) + \langle 2 \rangle_{2n|2n} \cdot P_{M,2} \\ &+ 2P_{M,2} + M. \end{aligned} \quad (\text{A6})$$

The two-particle correlations  $\langle 2 \rangle_{n|n}$  were already expressed in terms of the  $Q$  vector evaluated in harmonic  $n$  [see Eq. (16)]:

$$\langle 2 \rangle_{2n|2n} = \frac{|Q_{2n}|^2 - M}{P_{M,2}}. \quad (\text{A7})$$

To obtain  $\langle 3 \rangle_{2n|n,n}$  and  $\langle 3 \rangle_{n,n|2n}$  we have to decompose

$$\begin{aligned} Q_{2n} Q_n^* Q_n^* &= \langle 3 \rangle_{2n|n,n} \cdot P_{M,3} + \langle 2 \rangle_{n|n} \cdot 2P_{M,2} \\ &+ \langle 2 \rangle_{2n|2n} \cdot P_{M,2} + 1 \cdot M, \end{aligned} \quad (\text{A8})$$

and  $Q_n Q_n Q_{2n}^*$ . After inserting results for  $\langle 2 \rangle_{n|n}$  and  $\langle 2 \rangle_{2n|2n}$  given in Eqs. (16) and (A7), we arrive at the following equality:

$$\begin{aligned} \langle 3 \rangle_{n,n|2n} + \langle 3 \rangle_{2n|n,n} &= 2 \frac{\text{Re}[Q_{2n} Q_n^* Q_n^*] - 2 \cdot |Q_n|^2}{M(M-1)(M-2)} \\ &- 2 \frac{|Q_{2n}|^2 - 2M}{M(M-1)(M-2)}. \end{aligned} \quad (\text{A9})$$

After inserting Eqs. (16), (A7), and (A9) into Eq. (A6) and solving the resulting expression for  $\langle 4 \rangle_{n,n|n,n}$ , the single-event average four-particle correlations [Eq. (18)] follows.

This derivation can be generalized to obtain analytic results for any higher-order multiparticle azimuthal correlations. Below we provide the expression for the six-particle

correlation:

$$\begin{aligned} \langle 6 \rangle &\equiv \frac{1}{P_{M,6}} \sum_{i,j,k,l,m,n=1}^M e^{in(\phi_i + \phi_j + \phi_k - \phi_l - \phi_m - \phi_n)} \\ &= \frac{|Q_n|^6 + 9 \cdot |Q_{2n}|^2 |Q_n|^2 - 6 \cdot \text{Re}[Q_{2n} Q_n Q_n^* Q_n^* Q_n^*]}{M(M-1)(M-2)(M-3)(M-4)(M-5)} \\ &+ 4 \frac{\text{Re}[Q_{3n} Q_n^* Q_n^* Q_n^*] - 3 \cdot \text{Re}[Q_{3n} Q_{2n}^* Q_n^*]}{M(M-1)(M-2)(M-3)(M-4)(M-5)} \\ &+ 2 \frac{9(M-4) \cdot \text{Re}[Q_{2n} Q_n^* Q_n^*] + 2 \cdot |Q_{3n}|^2}{M(M-1)(M-2)(M-3)(M-4)(M-5)} \\ &- 9 \frac{|Q_n|^4 + |Q_{2n}|^2}{M(M-1)(M-2)(M-3)(M-5)} \\ &+ 18 \frac{|Q_n|^2}{M(M-1)(M-3)(M-4)} \\ &- \frac{6}{(M-1)(M-2)(M-3)}. \end{aligned} \quad (\text{A10})$$

With that, the sixth-order cumulant is given by

$$c_n\{6\} = \langle\langle 6 \rangle\rangle - 9 \cdot \langle\langle 2 \rangle\rangle \langle\langle 4 \rangle\rangle + 12 \cdot \langle\langle 2 \rangle\rangle^3, \quad (\text{A11})$$

and the reference flow  $v_n$  is estimated as

$$v_n\{6\} = \sqrt[6]{\frac{1}{4} c_n\{6\}}. \quad (\text{A12})$$

### APPENDIX B: PARTICLE WEIGHTS

Below we provide formulas to use for the case when the reference flow is calculated using particle weights. For that we introduce a weighted  $Q$  vector evaluated in harmonic  $n$ :

$$Q_{n,k} \equiv \sum_{i=1}^M w_i^k e^{in\phi_i}, \quad (\text{B1})$$

where  $w_i$  is a particle weight of the  $i$ th particle labeled as RFP and  $M$  is the total number of RFPs in an event. In general, we will need flow vectors with power  $k$  up to the order of multiparticle correlations. Similarly, we define

$$p_{n,k} \equiv \sum_{i=1}^{m_p} w_i^k e^{in\psi_i}. \quad (\text{B2})$$

Note that only particles which have a RFP label, have a nonunit weight, while for the particles labeled as POI *only*,  $w_i = 1$ . For the subset of POIs which consists of all particles labeled *both* as POI and RFP ( $m_q$  in total) we introduce

$$q_{n,k} \equiv \sum_{i=1}^{m_q} w_i^k e^{in\psi_i}. \quad (\text{B3})$$

For RFPs we also introduce

$$S_{p,k} \equiv \left[ \sum_{i=1}^M w_i^k \right]^p, \quad (\text{B4})$$

$$\mathcal{M}_{abcd\dots} \equiv \sum_{i,j,k,l,\dots=1}^M w_i^a w_j^b w_k^c w_l^d \dots \quad (\text{B5})$$

For all particles labeled *both* as RFP and POI we evaluate the following quantity:

$$s_{p,k} \equiv \left[ \sum_{i=1}^{m_q} w_i^k \right]^p, \quad (\text{B6})$$

while in the definition below the first sum runs over all POIs in the window of interest and the remaining sums run over all RPs in an event

$$\mathcal{M}'_{abcd\dots} \equiv \sum_{i=1}^{m_p} \sum_{j,k,l,\dots=1}^M w_i^a w_j^b w_k^c w_l^d \dots \quad (\text{B7})$$

Using the definitions presented above the *weighted* single-event two- and four-particle correlations are given by

$$\langle 2 \rangle \equiv \frac{1}{\mathcal{M}_{11}} \sum_{i,j=1}^M w_i w_j e^{in(\phi_i - \phi_j)}, \quad (\text{B8})$$

$$\langle 4 \rangle \equiv \frac{1}{\mathcal{M}_{1111}} \sum_{i,j,k,l=1}^M w_i w_j w_k w_l e^{in(\phi_i + \phi_j - \phi_k - \phi_l)}. \quad (\text{B9})$$

The event weights (9) and (10) now read

$$W_{(2)} \equiv \mathcal{M}_{11}, \quad (\text{B10})$$

$$W_{(4)} \equiv \mathcal{M}_{1111}. \quad (\text{B11})$$

Analogously, the reduced single-event multiparticle correlations now read

$$\langle 2' \rangle \equiv \frac{1}{\mathcal{M}'_{01}} \sum_{i=1}^{m_p} \sum_{j=1}^M w_j e^{in(\psi_i - \phi_j)}, \quad (\text{B12})$$

$$\langle 4' \rangle \equiv \frac{1}{\mathcal{M}'_{0111}} \sum_{i=1}^{m_p} \sum_{j,k,l=1}^M w_j w_k w_l e^{in(\psi_i + \phi_j - \phi_k - \phi_l)}, \quad (\text{B13})$$

where the event weights (24) and (25) are now

$$w_{(2')} \equiv \mathcal{M}'_{01}, \quad w_{(4')} \equiv \mathcal{M}'_{0111}. \quad (\text{B14})$$

The weighted average two-particle correlations are given by the following equations:

$$\begin{aligned} \langle 2 \rangle &= \frac{|Q_{n,1}|^2 - S_{1,2}}{S_{2,1} - S_{1,2}}, \\ \langle\langle 2 \rangle\rangle &= \frac{\sum_{i=1}^N (\mathcal{M}_{11})_i \langle 2 \rangle_i}{\sum_{i=1}^N (\mathcal{M}_{11})_i}, \\ \mathcal{M}_{11} &\equiv \sum_{i,j=1}^M w_i w_j \\ &= S_{2,1} - S_{1,2}, \end{aligned} \quad (\text{B15})$$

and the weighted average four-particle correlations are given by

$$\begin{aligned} \langle 4 \rangle &= [ |Q_{n,1}|^4 + |Q_{2n,2}|^2 - 2 \cdot \text{Re}[Q_{2n,2} Q_{n,1}^* Q_{n,1}^*] \\ &\quad + 8 \cdot \text{Re}[Q_{n,3} Q_{n,1}^*] - 4 \cdot S_{1,2} |Q_{n,1}|^2 \\ &\quad - 6 \cdot S_{1,4} - 2 \cdot S_{2,2} ] / \mathcal{M}_{1111}, \\ \mathcal{M}_{1111} &\equiv \sum_{i,j,k,l=1}^M w_i w_j w_k w_l \\ &= S_{4,1} - 6 \cdot S_{1,2} S_{2,1} + 8 \cdot S_{1,3} S_{1,1} + 3 \cdot S_{2,2} - 6 \cdot S_{1,4}, \\ \langle\langle 4 \rangle\rangle &= \frac{\sum_{i=1}^N (\mathcal{M}_{1111})_i \langle 4 \rangle_i}{\sum_{i=1}^N (\mathcal{M}_{1111})_i}, \end{aligned} \quad (\text{B16})$$

where the weighted  $Q$  vector,  $Q_{n,k}$ , was defined in Eq. (B1) and  $S_{p,k}$  in Eq. (B4).

Weighted reduced two- and four-particle azimuthal correlations are given by the following formulas:

$$\begin{aligned} \langle 2' \rangle &= \frac{p_{n,0} Q_{n,1}^* - S_{1,1}}{m_p S_{1,1} - s_{1,1}}, \\ \langle\langle 2' \rangle\rangle &= \frac{\sum_{i=1}^N (\mathcal{M}'_{01})_i \langle 2' \rangle_i}{\sum_{i=1}^N (\mathcal{M}'_{01})_i}, \\ \mathcal{M}'_{01} &\equiv \sum_{i=1}^{m_p} \sum_{j=1}^M w_j = m_p S_{1,1} - s_{1,1}, \end{aligned} \quad (\text{B17})$$

and

$$\begin{aligned} \langle 4' \rangle &= [ p_{n,0} Q_{n,1} Q_{n,1}^* Q_{n,1}^* - q_{2n,1} Q_{n,1}^* Q_{n,1}^* \\ &\quad - p_{n,0} Q_{n,1} Q_{2n,2}^* - 2 \cdot S_{1,2} p_{n,0} Q_{n,1}^* - 2 \cdot s_{1,1} |Q_{n,1}|^2 \\ &\quad + 7 \cdot q_{n,2} Q_{n,1}^* - Q_{n,1} q_{n,2}^* + q_{2n,1} Q_{2n,2}^* \\ &\quad + 2 \cdot p_{n,0} Q_{n,3}^* + 2 \cdot s_{1,1} S_{1,2} - 6 \cdot s_{1,3} ] / \mathcal{M}'_{0111}, \\ \langle\langle 4' \rangle\rangle &= \frac{\sum_{i=1}^N (\mathcal{M}'_{0111})_i \langle 4' \rangle_i}{\sum_{i=1}^N (\mathcal{M}'_{0111})_i}, \\ \mathcal{M}'_{0111} &\equiv \sum_{i=1}^{m_p} \sum_{j,k,l=1}^M w_j w_k w_l \\ &= m_p [ S_{3,1} - 3 \cdot S_{1,1} S_{1,2} + 2 \cdot S_{1,3} ] - 3 \cdot [ s_{1,1} (S_{2,1} \\ &\quad - S_{1,2}) + 2 \cdot (s_{1,3} - s_{1,2} S_{1,1}) ]. \end{aligned} \quad (\text{B18})$$

We note that to evaluate all quantities appearing on the right-hand sides in analytic expressions (B15)–(B18) only a single loop over data is required.

### APPENDIX C: NONUNIFORM ACCEPTANCE

Building cumulants from multiparticle correlations we have so far omitted terms which vanish for the detectors with uniform acceptance. For a more general case they have to be kept [7,8,20,25]. The more general second-order cumulant now reads

$$c_n \{2\} = \langle\langle 2 \rangle\rangle - [ \langle\langle \cos n\phi_1 \rangle\rangle^2 + \langle\langle \sin n\phi_1 \rangle\rangle^2 ]. \quad (\text{C1})$$

The correction terms can be expressed in terms of the real and imaginary parts of the  $Q$  vector (4):

$$\langle\langle \cos n\phi_1 \rangle\rangle = \frac{\sum_{i=1}^N (\text{Re}[Q_n])_i}{\sum_{i=1}^N M_i}, \quad (\text{C2})$$

$$\langle\langle \sin n\phi_1 \rangle\rangle = \frac{\sum_{i=1}^N (\text{Im}[Q_n])_i}{\sum_{i=1}^N M_i}. \quad (\text{C3})$$

When particle weights are used the average two-particle correlation  $\langle\langle 2 \rangle\rangle$  is determined from Eqs. (B15), while Eqs. (C2) and (C3) generalize into

$$\langle\langle \cos n\phi_1 \rangle\rangle = \frac{\sum_{i=1}^N (\text{Re}[Q_n])_i}{\sum_{i=1}^N (S_{1,1})_i}, \quad (\text{C4})$$



$$\langle\langle \sin n\phi_1 \rangle\rangle = \frac{\sum_{i=1}^N (\text{Im}[Q_{n,1}]_i)}{\sum_{i=1}^N (S_{1,1})_i}, \quad (\text{C5})$$

where  $Q_{n,1}$  can be determined from the definition of the weighted  $Q$  vector (B1) and  $S_{1,1}$  from definition (B4).

The generalized fourth-order cumulant reads

$$\begin{aligned} c_n\{4\} = & \langle\langle 4 \rangle\rangle - 2 \cdot \langle\langle 2 \rangle\rangle^2 \\ & - 4 \cdot \langle\langle \cos n\phi_1 \rangle\rangle \langle\langle \cos n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle \\ & + 4 \cdot \langle\langle \sin n\phi_1 \rangle\rangle \langle\langle \sin n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle \\ & - \langle\langle \cos n(\phi_1 + \phi_2) \rangle\rangle^2 - \langle\langle \sin n(\phi_1 + \phi_2) \rangle\rangle^2 \\ & + 4 \cdot \langle\langle \cos n(\phi_1 + \phi_2) \rangle\rangle [\langle\langle \cos n\phi_1 \rangle\rangle^2 - \langle\langle \sin n\phi_1 \rangle\rangle^2] \\ & + 8 \cdot \langle\langle \sin n(\phi_1 + \phi_2) \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle \\ & + 8 \cdot \langle\langle \cos n(\phi_1 - \phi_2) \rangle\rangle [\langle\langle \cos n\phi_1 \rangle\rangle^2 + \langle\langle \sin n\phi_1 \rangle\rangle^2] \\ & - 6 \cdot [\langle\langle \cos n\phi_1 \rangle\rangle^2 + \langle\langle \sin n\phi_1 \rangle\rangle^2]^2. \end{aligned} \quad (\text{C6})$$

The terms starting from the second line in Eq. (C6) counterbalance the bias coming from nonuniform acceptance so that  $c_n\{4\}$  is unbiased. These terms can be expressed in terms of  $Q$  vectors:

$$\langle\langle \cos n(\phi_1 + \phi_2) \rangle\rangle = \frac{\sum_{i=1}^N (\text{Re}[Q_n Q_n - Q_{2n}]_i)}{\sum_{i=1}^N M_i (M_i - 1)}, \quad (\text{C7})$$

$$\langle\langle \sin n(\phi_1 + \phi_2) \rangle\rangle = \frac{\sum_{i=1}^N (\text{Im}[Q_n Q_n - Q_{2n}]_i)}{\sum_{i=1}^N M_i (M_i - 1)}, \quad (\text{C8})$$

$$\begin{aligned} \langle\langle \cos n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle = & \left\{ \sum_{i=1}^N (\text{Re}[Q_n Q_n^* Q_n^* - Q_n Q_{2n}^*] \right. \\ & \left. - 2(M-1)\text{Re}[Q_n^*]_i) \right\} / \sum_{i=1}^N M_i \\ & \times (M_i - 1)(M_i - 2), \end{aligned} \quad (\text{C9})$$

$$\begin{aligned} \langle\langle \sin n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle = & \left\{ \sum_{i=1}^N (\text{Im}[Q_n Q_n^* Q_n^* - Q_n Q_{2n}^*] \right. \\ & \left. - 2(M-1)\text{Im}[Q_n^*]_i) \right\} / \sum_{i=1}^N M_i \\ & \times (M_i - 1)(M_i - 2). \end{aligned} \quad (\text{C10})$$

When particle weights are used the average two-particle correlation  $\langle\langle 2 \rangle\rangle$  is determined from Eqs. (B15), the average four-particle correlation  $\langle\langle 4 \rangle\rangle$  is determined from Eqs. (B16), Eqs. (C7) and (C8) generalize into

$$\begin{aligned} \langle\langle \cos n(\phi_1 + \phi_2) \rangle\rangle &= \frac{\sum_{i=1}^N (\text{Re}[Q_{n,1} Q_{n,1} - Q_{2n,2}]_i)}{\sum_{i=1}^N (\mathcal{M}_{11})_i}, \\ \langle\langle \sin n(\phi_1 + \phi_2) \rangle\rangle &= \frac{\sum_{i=1}^N (\text{Im}[Q_{n,1} Q_{n,1} - Q_{2n,2}]_i)}{\sum_{i=1}^N (\mathcal{M}_{11})_i}, \\ \mathcal{M}_{11} &\equiv \sum_{i,j=1}^M w_i w_j = S_{2,1} - S_{1,2}, \end{aligned} \quad (\text{C11})$$

and Eqs. (C9) and (C10) generalize into

$$\begin{aligned} & \langle\langle \cos n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle \\ &= \left\{ \sum_{i=1}^N (\text{Re}[Q_{n,1} Q_{n,1}^* Q_{n,1}^* - Q_{n,1} Q_{2n,2}^* - 2 \cdot S_{1,2} Q_{n,1}^* \right. \\ & \quad \left. + 2 \cdot Q_{n,3}^*]_i) \right\} / \sum_{i=1}^N (\mathcal{M}_{111})_i, \\ & \langle\langle \sin n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle \\ &= \left\{ \sum_{i=1}^N (\text{Im}[Q_{n,1} Q_{n,1}^* Q_{n,1}^* - Q_{n,1} Q_{2n,2}^* - 2 \cdot S_{1,2} Q_{n,1}^* \right. \\ & \quad \left. + 2 \cdot Q_{n,3}^*]_i) \right\} / \sum_{i=1}^N (\mathcal{M}_{111})_i, \\ \mathcal{M}_{111} &\equiv \sum_{i,j,k=1}^M w_i w_j w_k = S_{3,1} - 3 \cdot S_{1,2} S_{1,1} + 2 \cdot S_{1,3}. \end{aligned} \quad (\text{C12})$$

The generalized second-order differential cumulant reads

$$\begin{aligned} d_n\{2\} = & \langle\langle 2' \rangle\rangle - \langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \cos n\phi_2 \rangle\rangle \\ & - \langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \sin n\phi_2 \rangle\rangle. \end{aligned} \quad (\text{C13})$$

Expressions for  $\langle\langle \cos n\phi_1 \rangle\rangle$  and  $\langle\langle \sin n\phi_1 \rangle\rangle$  were already given in Eqs. (C2) and (C3), respectively [when particle weights are being used in Eqs. (C4) and (C5), respectively]. Similarly,

$$\langle\langle \cos n\psi_1 \rangle\rangle = \frac{\sum_{i=1}^N (\text{Re}[p_n]_i)}{\sum_{i=1}^N (m_p)_i}, \quad (\text{C14})$$

$$\langle\langle \sin n\psi_1 \rangle\rangle = \frac{\sum_{i=1}^N (\text{Im}[p_n]_i)}{\sum_{i=1}^N (m_p)_i}, \quad (\text{C15})$$

where  $p_n$  and  $m_p$  were defined in Sec. IV. Equations (C14) and (C15) remain unchanged when particle weights are being used.

The generalized fourth-order differential cumulant reads

$$\begin{aligned} d_n\{4\} = & \langle\langle 4' \rangle\rangle - 2 \cdot \langle\langle 2' \rangle\rangle \langle\langle 2 \rangle\rangle \\ & - \langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \cos n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle \\ & + \langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \sin n(\phi_1 - \phi_2 - \phi_3) \rangle\rangle \\ & - \langle\langle \cos n\phi_1 \rangle\rangle \langle\langle \cos n(\psi_1 - \phi_2 - \phi_3) \rangle\rangle \\ & + \langle\langle \sin n\phi_1 \rangle\rangle \langle\langle \sin n(\psi_1 - \phi_2 - \phi_3) \rangle\rangle \\ & - 2 \cdot \langle\langle \cos n\phi_1 \rangle\rangle \langle\langle \cos n(\psi_1 + \phi_2 - \phi_3) \rangle\rangle \\ & - 2 \cdot \langle\langle \sin n\phi_1 \rangle\rangle \langle\langle \sin n(\psi_1 + \phi_2 - \phi_3) \rangle\rangle \\ & - \langle\langle \cos n(\psi_1 + \phi_2) \rangle\rangle \langle\langle \cos n(\phi_1 + \phi_2) \rangle\rangle \\ & - \langle\langle \sin n(\psi_1 + \phi_2) \rangle\rangle \langle\langle \sin n(\phi_1 + \phi_2) \rangle\rangle \\ & + 2 \cdot \langle\langle \cos n(\phi_1 + \phi_2) \rangle\rangle [\langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle \\ & - \langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle] + 2 \cdot \langle\langle \sin n(\phi_1 + \phi_2) \rangle\rangle \\ & \times [\langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle + \langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle] \\ & + 4 \cdot \langle\langle \cos n(\phi_1 - \phi_2) \rangle\rangle \\ & \times [\langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle + \langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle] \\ & + 2 \cdot \langle\langle \cos n(\psi_1 + \phi_2) \rangle\rangle \end{aligned}$$

$$\begin{aligned}
 & \times [\langle\langle \cos n\phi_1 \rangle\rangle^2 - \langle\langle \sin n\phi_1 \rangle\rangle^2] \\
 & + 4 \cdot \langle\langle \sin n(\psi_1 + \phi_2) \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle \\
 & + 4 \cdot \langle\langle \cos n(\psi_1 - \phi_2) \rangle\rangle [\langle\langle \cos n\phi_1 \rangle\rangle^2 + \langle\langle \sin n\phi_1 \rangle\rangle^2] \\
 & - 6 \cdot [\langle\langle \cos n\phi_1 \rangle\rangle^2 - \langle\langle \sin n\phi_1 \rangle\rangle^2] \\
 & \times [\langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle - \langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle] \\
 & - 12 \cdot \langle\langle \cos n\phi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle [\langle\langle \sin n\psi_1 \rangle\rangle \langle\langle \cos n\phi_1 \rangle\rangle \\
 & + \langle\langle \cos n\psi_1 \rangle\rangle \langle\langle \sin n\phi_1 \rangle\rangle]. \tag{C16}
 \end{aligned}$$

The terms starting from the second line in Eq. (C16) counter-balance the bias coming from nonuniform acceptance. Some of the new terms appearing in this expression can be expressed again in products of flow vectors:

$$\begin{aligned}
 \langle\langle \cos n(\psi_1 + \phi_2) \rangle\rangle &= \frac{\sum_{i=1}^N (\text{Re}[p_n Q_n - q_{2n}]_i)}{\sum_{i=1}^N (m_p M - m_q)_i}, \\
 \langle\langle \sin n(\psi_1 + \phi_2) \rangle\rangle &= \frac{\sum_{i=1}^N (\text{Im}[p_n Q_n - q_{2n}]_i)}{\sum_{i=1}^N (m_p M - m_q)_i}, \tag{C17}
 \end{aligned}$$

$$\begin{aligned}
 \langle\langle \cos n(\psi_1 + \phi_2 - \phi_3) \rangle\rangle &= \left\{ \sum_{i=1}^N (\text{Re}[p_n(|Q_n|^2 - M)] - \text{Re}[q_{2n} Q_n^* + m_q Q_n - 2q_n]_i) \right\} / \left\{ \sum_{i=1}^N [(m_p M - 2m_q)(M - 1)]_i \right\}, \\
 \langle\langle \sin n(\psi_1 + \phi_2 - \phi_3) \rangle\rangle &= \left\{ \sum_{i=1}^N (\text{Im}[p_n(|Q_n|^2 - M)] - \text{Im}[q_{2n} Q_n^* + m_q Q_n - 2q_n]_i) \right\} / \left\{ \sum_{i=1}^N [(m_p M - 2m_q)(M - 1)]_i \right\}, \tag{C18}
 \end{aligned}$$

$$\begin{aligned}
 \langle\langle \cos n(\psi_1 - \phi_2 - \phi_3) \rangle\rangle &= \left\{ \sum_{i=1}^N (\text{Re}[p_n Q_n^* Q_n^* - p_n Q_{2n}^*] - \text{Re}[2m_q Q_n^* - 2q_n^*]_i) \right\} / \left\{ \sum_{i=1}^N [(m_p M - 2m_q)(M - 1)]_i \right\}, \\
 \langle\langle \sin n(\psi_1 - \phi_2 - \phi_3) \rangle\rangle &= \left\{ \sum_{i=1}^N (\text{Im}[p_n Q_n^* Q_n^* - p_n Q_{2n}^*] - \text{Im}[2m_q Q_n^* - 2q_n^*]_i) \right\} / \left\{ \sum_{i=1}^N [(m_p M - 2m_q)(M - 1)]_i \right\}. \tag{C19}
 \end{aligned}$$

When particle weights are used Eqs. (C17) generalize into

$$\langle\langle \sin n(\psi_1 + \phi_2) \rangle\rangle = \frac{\sum_{i=1}^N (\text{Im}[p_n Q_{n,k} - q_{2n,k}]_i)}{\sum_{i=1}^N (m_p S_{1,1} - s_{1,1})_i}, \tag{C20}$$

$$\langle\langle \cos n(\psi_1 + \phi_2) \rangle\rangle = \frac{\sum_{i=1}^N (\text{Re}[p_n Q_{n,k} - q_{2n,k}]_i)}{\sum_{i=1}^N (m_p S_{1,1} - s_{1,1})_i},$$

Eqs. (C18) generalize into

$$\begin{aligned}
 & \langle\langle \cos n(\psi_1 + \phi_2 - \phi_3) \rangle\rangle \\
 &= \left\{ \sum_{i=1}^N (\text{Re}[p_n(|Q_{n,1}|^2 - S_{1,2})] - \text{Re}[q_{2n,1} Q_{n,1}^* + s_{1,1} Q_{n,1} - 2q_{n,2}]_i) \right\} / \left\{ \sum_{i=1}^N (m_p(S_{2,1} - S_{1,2}) - 2 \cdot (s_{1,1} S_{1,1} - s_{1,2}))_i \right\}, \\
 & \langle\langle \sin n(\psi_1 + \phi_2 - \phi_3) \rangle\rangle \\
 &= \left\{ \sum_{i=1}^N (\text{Im}[p_n(|Q_{n,1}|^2 - S_{1,2})] - \text{Im}[q_{2n,1} Q_{n,1}^* + s_{1,1} Q_{n,1} - 2q_{n,2}]_i) \right\} / \left\{ \sum_{i=1}^N (m_p(S_{2,1} - S_{1,2}) - 2 \cdot (s_{1,1} S_{1,1} - s_{1,2}))_i \right\}, \tag{C21}
 \end{aligned}$$

and finally, Eqs. (C19) generalize into

$$\begin{aligned}
 & \langle\langle \cos n(\psi_1 - \phi_2 - \phi_3) \rangle\rangle \\
 &= \left\{ \sum_{i=1}^N (\text{Re}[p_n(Q_{n,1}^* Q_{n,1}^* - Q_{2n,2}^*)] - 2 \cdot \text{Re}[s_{1,1} Q_{n,1}^* - q_{n,2}^*]_i) \right\} / \left\{ \sum_{i=1}^N (m_p(S_{2,1} - S_{1,2}) - 2 \cdot (s_{1,1} S_{1,1} - s_{1,2}))_i \right\}, \\
 & \langle\langle \sin n(\psi_1 - \phi_2 - \phi_3) \rangle\rangle
 \end{aligned}$$

$$= \left\{ \sum_{i=1}^N (\text{Im}[p_n(Q_{n,1}^* Q_{n,1}^* - Q_{2n,2}^*)] - 2 \cdot \text{Im}[s_{1,1} Q_{n,1}^* - q_{n,2}^*])_i \right\} / \left\{ \sum_{i=1}^N (m_p(S_{2,1} - S_{1,2}) - 2 \cdot (s_{1,1} S_{1,1} - s_{1,2}))_i \right\}. \quad (\text{C22})$$

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