

Melting behaviour of molecular mixed crystalline materials: measurement with adiabatic calorimetry and modelling using ULTRACAL

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The melting behaviour of binary mixed crystalline materials was measured with adiabatic calorimetry. The experimental results (heat capacity against temperature graphs) are explained in terms of a model that is based on the assumption that the inhomogeneity of the materials can be described by a Gaussian distribution function. Although this model, called ULTRACAL, has only one adjustable parameter, it is capable of reproducing the experimental data with a good degree of accuracy, as demonstrated for various samples of (1,4-dichlorobenzene + 1,4-dibromobenzene). ULTRACAL thus provides a link between the adiabatic calorimetry data and the solid–liquid T_x phase diagram. It is shown that the model can be used for the determination of phase diagrams. By using ULTRACAL to assess the heat capacity against temperature graphs of five samples, the solid–liquid T_x phase diagram of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) was determined.

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1. Introduction

A mixed crystalline material, in going from a solid to a liquid state, gives rise ideally to the type of heat capacity against temperature graph (c_p-T) shown in figure 1. The sharp rise at the solidus temperature and sharp fall at the liquidus temperature allow the phase diagram characteristics for a given composition to be determined.

In practice, however, the ideal c_p-T graph is hardly ever observed. The extent to which it can be approximated depends upon experimental procedures and particularly upon the degree of homogeneity of the sample, *i.e.* the way in which the sample was prepared. Because of low solid-state diffusion rates,⁽¹⁾ mixed crystalline samples of molecular substances have to be prepared starting with a fluid phase: melt, vapour or solution in a

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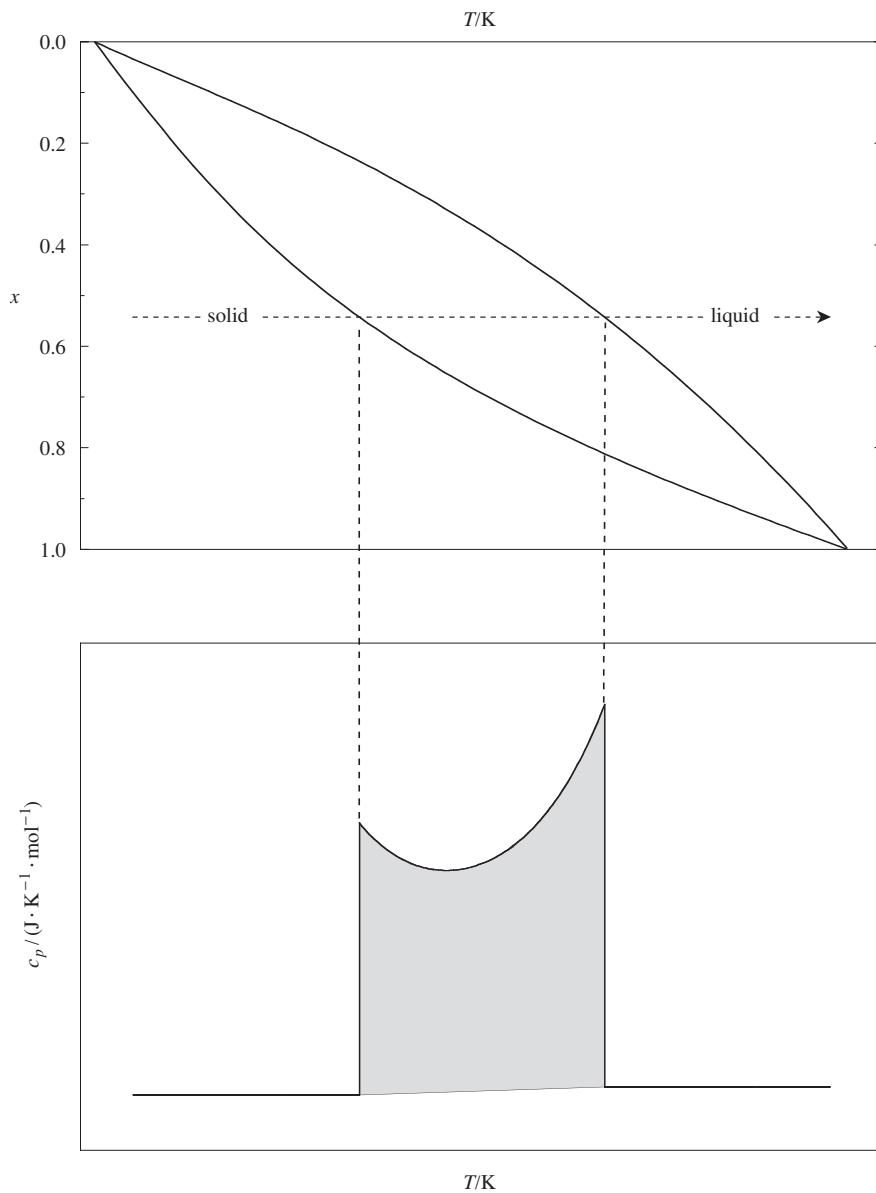


FIGURE 1. Relation between the solid–liquid Tx phase diagram of a binary mixture (upper graph) and the theoretical ideal c_p – T graph (lower graph). The shaded area in the lower graph corresponds to the heat of melting for the given composition.

solvent. The necessity of using a fluid medium, however, has unavoidable adverse effects on the degree of homogeneity of the material (as, from an equilibrium point of view,

the transition from one mixed state, the fluid medium, to the mixed crystalline state is accompanied by a change in composition).

In searching for standardisation of sample preparation procedures, our group, particularly in the initial phase of its existence, explored the possibilities of the zone levelling technique. A zone levelling instrument was designed by Kolkert and its performance was tested on (naphthalene + β -naphthol).^(2,3) The method of zone levelling exceeded our expectations. It yielded solidus and liquidus data in good agreement with the results of thermodynamic analysis of phase diagrams and thermochemical data. Similar results were obtained by Bouwstra for (*trans*-diphenylethene + *trans*-azobenzene).⁽⁴⁾

Zone levelling provided a solid basis for examining the possibilities and limitations of less sophisticated methods of sample preparation such as quenching from a melt or rapid co-precipitation from a solution in a highly volatile solvent. These relatively simple methods allow the preparation of 5 g samples of mixed crystalline material in about half an hour, against half a month in the case of zone levelling. This paper focuses on the method of rapid co-precipitation from solution and its application to (1,4-dichlorobenzene + 1,4-dibromobenzene) and (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene).

In figure 2 three examples of c_p-T graphs corresponding to the same mean composition ($x_m = 0.52$) for (1,4-dichlorobenzene + 1,4-dibromobenzene) are given. As can be seen, c_p-T graphs may cover a spectrum of shapes: from the ideal graph, the solid curve, when the compositional homogeneity is 100 per cent, to the graph represented by open squares. The latter was obtained using a sample prepared by quenching a liquid mixture. It is clear that the material consists of regions with different compositions covering a large part of the mole fraction range; see also Bouwstra.⁽⁴⁾ The full circles in figure 2 represent the experimental results for a sample prepared by co-precipitation from solution. The shape of the curve does suggest that the degree of homogeneity is rather high but, unfortunately, shows also that direct and accurate information on the phase diagram cannot be extracted. Therefore we have decided to explore the use of a method, a mathematical model for describing the inhomogeneity of the sample, for determining accurately solidus and liquidus temperatures without the need for input data other than those on pure substances and mixing properties.

The investigations⁽⁵⁾ were carried out as follows. Initially, the known solid–liquid T_x phase diagram of (1,4-dichlorobenzene + 1,4-dibromobenzene) was used to test the adopted model. Secondly, the model was taken as the starting point for an iterative procedure by which a limited set of experimental c_p-T graphs of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) were interpreted and the (unknown) solid–liquid T_x phase diagram was established. Lastly, and guided by the outcome of the model calculations, the possibility of determining solidus and liquidus temperatures directly from c_p-T graphs, *i.e.* without using the mathematical procedure, was examined.

2. Materials

The substances 1,4-dichlorobenzene, 1,4-dibromobenzene, 1,3,5-trichlorobenzene, and 1,3,5-tribromobenzene were obtained from Aldrich Chemical Co. Inc., Milwaukee, WI, U.S.A. 1,4-Dichlorobenzene and 1,3,5-trichlorobenzene were purified by sublimation

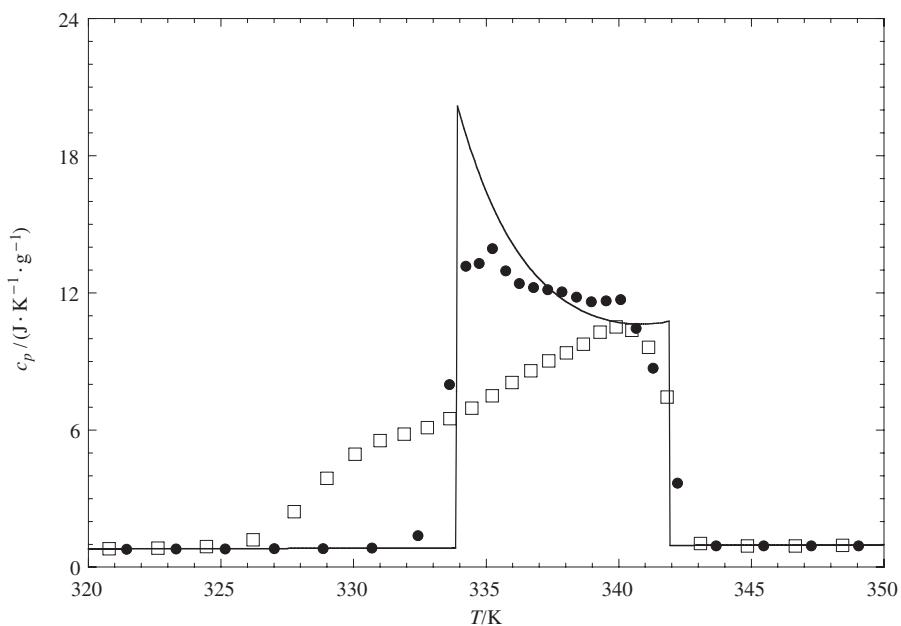


FIGURE 2. Examples of c_p - T graphs at the mean composition $x_m = 0.52$ for (1,4-dichlorobenzene + 1,4-dibromobenzene): ●, sample prepared by co-precipitation from solution; □, sample prepared by quenching of a liquid mixture; —, theoretical ideal c_p - T graph. Calculations were performed with heat capacity expressed in $J \cdot K^{-1} \cdot g^{-1}$. In this way the error due to conversion of the experimental heat capacity data to $J \cdot K^{-1} \cdot mol^{-1}$ using the average molar mass can be avoided. All data presented in figures 2–6 are available in tabular form upon request. In addition, the computer program ULTRACAL can be obtained from the authors.

in vacuo under continuous evacuation at approximately 1 Pa. For the other substances this purification method did not yield satisfactory results.

1,4-Dibromobenzene (light-brown coloured) was dissolved in ethanol. 200 ml of the saturated solution were filtered and poured into four litres of distilled water. The precipitate was dried at $p = 1$ Pa. Subsequently, the white substance was sublimated once.

Dark-brown coloured 1,3,5-tribromobenzene was sublimated once. The yellow product was further purified by recrystallization from ethanol. After centrifugation during three minutes at 2400 r.p.m., the substance was isolated and washed with a small amount of acetone. Finally, the product was dried *in vacuo*.

The purity of the substances was checked by means of adiabatic calorimetry. Except for 1,3,5-tribromobenzene (mole fraction purity = 0.9990), the mole fraction purities were found to be at least 0.9998.

PREPARATION OF MIXED SAMPLES

Mixed crystalline materials prepared by rapid co-precipitation from solution were used in the investigations. Pure substances in the desired proportions were dissolved in diethyl

ether and a mixed solid material was allowed to form through fast evaporation of the solvent, *i.e.* supersaturation was driven far enough for the whole mass to crystallize at about the same moment. In this way mixed crystalline materials were obtained within 30 min.

3. Experimental

All measurements were made using a partially reconstructed and improved version of the adiabatic calorimeter CAL V,⁽⁶⁾ the original construction of which was described extensively by van Miltenburg *et al.*⁽⁷⁾ and van Bommel.⁽⁸⁾

Each measurement consisted of successive heating periods and stabilization periods of 500 s and 3600 s duration, respectively. The stabilization periods were extended from the normal 1500 s to 3600 s in order to come closer to equilibrium.

4. The ULTRACAL model

The method of co-precipitation from solution yields a mixed crystalline material that is a fine powder, *i.e.* a collection of numerous very small crystallites. Furthermore, the product is formed within minutes which suggests a more or less random crystallization process. These two observations form the basis for the following three assumptions that underly the model called ULTRACAL (the name ULTRACAL is derived from *Calorimetrika Ultraiectina*, *Ultraiectum* being the Latin name for Utrecht):

(i) each of the numerous crystallites is homogeneous in composition and shows ideal melting behaviour, *i.e.* in accordance with figure 1; (ii) a given crystallite *i* has its own composition x_i , and the distribution of compositions in the sample as a whole is a Gaussian function around the mean composition (x_m); this distribution function is characterized by a standard deviation σ , referred to here as "dispersion"; (iii) there is no interaction between the crystallites, *i.e.* each crystallite melts independently and there is no mixing between the formed liquid phases.

Consequently, the c_p-T graph of the sample as a whole is the weighted sum of numerous ideal c_p-T graphs. Now let k represent the number of different compositions in the sample and M_i the ideal c_p-T graph corresponding to composition x_i , the c_p-T graph of the sample (M_T) can then be given as:

$$M_T = Z^{-1} \cdot \sum_{i=1}^k \exp\{-(x_i - x_m)^2 / 2 \cdot \sigma^2\} \cdot M_i, \quad (1)$$

where Z , the normalization constant, is given by

$$Z = \sum_{j=1}^k \exp\{-(x_j - x_m)^2 / 2 \cdot \sigma^2\}. \quad (2)$$

Using the pure substance data (table 1), the optimized phase diagram, and the excess enthalpy of melting (table 3), ULTRACAL calculations were carried out on c_p-T graphs of

TABLE 1. Molar thermodynamic properties of the pure substances 1,4-dichlorobenzene (diCl; $M = 147.00 \text{ g} \cdot \text{mol}^{-1}$), 1,4-dibromobenzene (diBr; $M = 235.91 \text{ g} \cdot \text{mol}^{-1}$), 1,3,5-trichlorobenzene (triCl; $M = 181.45 \text{ g} \cdot \text{mol}^{-1}$), and 1,3,5-tribromobenzene (triBr; $M = 314.80 \text{ g} \cdot \text{mol}^{-1}$). Heat capacity data c_p^0 are given at the reference temperature $\theta = 298.15 \text{ K}$ ($p^0 = 10^5 \text{ Pa}$; $R = 8.314472 \text{ J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$)⁽⁵⁾

Substance	$\frac{C_{p,m}^0(\text{cr}, \theta)}{R}$	$\frac{(\partial C_{p,m}^0 / \partial T)(\text{cr})}{R \cdot \text{K}^{-1}}$	$\frac{T_{\text{cr-1}}}{\text{K}}$	$\frac{\Delta_{\text{cr}}^1 H_m^0(T_{\text{cr-1}})}{R \cdot \text{K}}$	$\frac{C_{p,m}^0(1, \theta)}{R}$	$\frac{(\partial C_{p,m}^0 / \partial T)(1)}{R \cdot \text{K}^{-1}}$
diCl ^a	17.293	$5.326 \cdot 10^{-2}$	326.05	2168.2	20.368	$2.838 \cdot 10^{-2}$
diBr	17.480	$5.297 \cdot 10^{-2}$	360.48	2452.0	21.282	$2.601 \cdot 10^{-2}$
triCl	19.042	$4.637 \cdot 10^{-2}$	335.92	2111.7	22.761	$2.716 \cdot 10^{-2}$
triBr	19.432	$4.002 \cdot 10^{-2}$	394.95	2612.4	23.097	$3.578 \cdot 10^{-2}$

^a All data for crystalline 1,4-dichlorobenzene apply to the α -phase; the α -phase is stable up to $T = 306 \text{ K}$, see text.

TABLE 2. Solidus and liquidus temperatures (T^{sol} and T^{liq}) of the optimized Tx phase diagrams of (1,4-dichlorobenzene + 1,4-dibromobenzene) and (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene)

x	(1,4-dichlorobenzene + 1,3,5-tribromobenzene)		1,3,5-trichlorobenzene + 1,4-dibromobenzene		
	T^{sol}/K	T^{liq}/K	x	T^{sol}/K	T^{liq}/K
0.10	326.63	326.87	0.10	337.91	340.02
0.20	327.70	329.09	0.20	340.18	346.86
0.30	329.16	332.65	0.30	342.71	354.86
0.40	331.03	336.85	0.40	345.66	362.46
0.50	333.42	341.20	0.50	349.24	369.28
0.60	336.50	345.46	0.60	353.82	375.34
0.70	340.48	349.52	0.70	359.93	380.81
0.80	345.62	353.38	0.80	368.30	385.82
0.90	352.20	357.30	0.90	3879.84	390.49

six different samples. The outcome of the calculations is given in table 4. Typical examples of calculated c_p-T graphs along with experimental data are shown in figure 4.

In practice the compositions are assumed to range from $(x_m - 5 \cdot \sigma)$ to $(x_m + 5 \cdot \sigma)$, and the number of different compositions k is about 500. For calculating an ideal curve M_i the molar thermodynamic properties of the pure substances (molar heat capacities of the crystalline and liquid phases, temperature and molar enthalpy of melting), the molar excess enthalpy of melting and the solid–liquid Tx phase diagram (solidus and liquidus temperatures as a function of composition) are required as input.

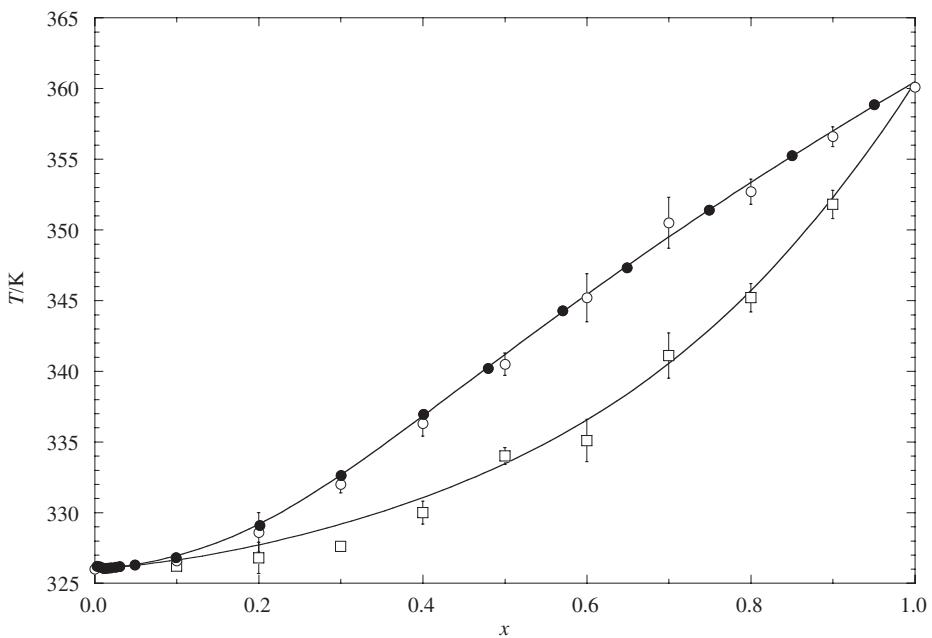


FIGURE 3. Solid (α)-liquid T_x phase diagram of (1,4-dichlorobenzene + 1,4-dibromobenzene): ●, liquidus data by Campbell and Prodan;⁽⁹⁾ ○, liquidus data by Haget *et al.*;⁽¹³⁾ □, solidus data by Haget *et al.*;⁽¹³⁾ —, phase diagram calculated using the following parameters of the excess Gibbs energy functions of equation type (3): ($g_0^1/J \cdot mol^{-1}$) = 0, ($g_1^1/J \cdot mol^{-1}$) = 0, ($g_0^S/J \cdot mol^{-1}$) = 1430, and ($g_1^S/J \cdot mol^{-1}$) = 349 and the data listed in table 1 (in the calculations the temperature dependence of the transition heat capacity of the pure substances was not taken into account).

TABLE 3. Molar excess enthalpy difference between the mixed crystalline state and mixed liquid state $\Delta_S^1 H^E$ of (1,4-dichlorobenzene + 1,4-dibromobenzene) and (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) derived from experimental c_p-T graphs of six samples expressed in terms of the parameters h_0 and h_1 as

$$\Delta_S^1 H^E(x) = x \cdot (1-x) \cdot \{h_0 + h_1 \cdot (1-2 \cdot x)\}$$

System	h_0 $J \cdot mol^{-1}$	h_1 $J \cdot mol^{-1}$
(1,4-dichlorobenzene + 1,4-dibromobenzene)	-1983	-346
(1,3,5-trichlorobenzene + 1,3,5-tribromobenzene)	-5709	1233

In modelling with ULTRACAL the dispersion σ is obtained by varying its value until a good agreement between the experimental and calculated c_p-T graphs is visually obtained. Although this procedure is not entirely free from subjectivity, the dispersion can be determined with adequate accuracy (the shape of the calculated graph is sensitive to

TABLE 4. Dispersion σ of six samples of (1,4-dichlorobenzene + 1,4-dibromobenzene) and five samples of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene). Apart from the samples with mean composition $x_m = 0.60$, which were prepared by zone levelling, all samples were prepared by co-precipitation from solution

(1,4-dichlorobenzene + 1,4-dibromobenzene)		(1,3,5-trichlorobenzene + 1,3,5-tribromobenzene)	
x_m	σ	x_m	σ
0.21	0.032	0.20	0.017
0.52	0.037	0.40	0.024
0.60	0.020	0.50	0.027
0.60	0.021	0.68	0.020
0.81	0.020	0.81	0.017
0.83	0.020		

changes in σ of the order ± 0.001). It may turn out, however, that it is impossible to obtain a good agreement on both the rising and falling edges of the graphs. In such a case, the rising edge of the experimental data was chosen as the target to match, since the third assumption of independently melting crystallites, *i.e.* no liquid–liquid mixing, is more realistic at the beginning than at the end of the melting process. For a detailed account of the ULTRACAL model and the calculation of ideal c_p-T graphs the reader is referred to van der Linde.⁽⁵⁾

5. Results

(1,4-DICHLOROBENZENE + 1,4-DIBROMOBENZENE)

As mentioned above, the solid–liquid T_x phase diagram is part of the input to ULTRACAL. In the case of (1,4-dichlorobenzene + 1,4-dibromobenzene) the liquidus, determined by Campbell and Prodan in 1948,⁽⁹⁾ is accurately known. As previously demonstrated,⁽¹⁰⁾ Campbell and Prodan's liquidus data are very accurate, but unfortunately their solidus data are not (the data have a systematic error, a common feature of solidus temperatures read from cooling curves). Therefore the solidus was obtained by calculation, using the LIQFIT method.^(4, 11, 12)

LIQFIT is an iterative procedure for phase-diagram calculations, in which the liquidus is made to pass through a set of experimental liquidus points. Apart from the experimental liquidus data, the input for LIQFIT consists of the thermodynamic properties of the pure substances and the excess Gibbs energy of either the mixed crystalline state (G^E, s) or the liquid state (G^E, l). As a rule, and in view of the relatively small temperature range of the solid–liquid region, the change of these excess Gibbs energies with temperature is neglected. The output of LIQFIT consists of (i) the calculated solidus, and (ii) the unknown

excess function. The excess functions are expressed in terms of the parameters (g_0 and g_1) as

$$G^E(x) = x \cdot (1 - x) \cdot \{g_0 + g_1 \cdot (1 - 2 \cdot x)\}. \quad (3)$$

The thermodynamic properties of the pure substances used for LIQFIT are given in table 1. Crystalline 1,4-dibromobenzene is isomorphous with the α -form of 1,4-dichlorobenzene (monoclinic). At temperatures above 306 K the stable form of 1,4-dichlorobenzene is triclinic (β), which has a melting point 0.19 K higher than the metastable melting point of the α -form. In the context of this work, however, the existence of the β -form and its small single-phase field can be ignored.

Measurements of the excess properties of this system⁽⁵⁾ have shown that, within the experimental uncertainties, the mixed liquid state can be treated as an ideal mixture. Accordingly, and in terms of equation (3), the computations were made with $g_0^l = 0$ and $g_1^l = 0$ as the parameters of the known function, and g_0^s and g_1^s as the parameters to be adjusted. The phase diagram obtained by LIQFIT, using Campbell and Prodan's liquidus data as input, is depicted in figure 3, along with the input data and the solidus and liquidus data of Haget *et al.*⁽¹³⁾ The latter were determined by means of differential thermal analysis d.t.a. using samples prepared by co-precipitation from solution (the liquidus temperatures determined by Haget *et al.* are systematically 0.35 K lower than the data of Campbell and Prodan). In table 2 calculated solidus and liquidus temperatures are given for mole fraction steps of 0.1 from $x = 0.0$ to $x = 1.0$. The calculated excess Gibbs energy of the mixed crystalline state, $G^{E,s}$, according to equation (3), is $g_0^s = 1430 \text{ J} \cdot \text{mol}^{-1}$ and $g_1^s = 349 \text{ J} \cdot \text{mol}^{-1}$.

(1,3,5-TRICHLOROBENZENE + 1,3,5-TRIBROMOBENZENE)

In the case of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) the objective was to determine the unknown solid–liquid T_x phase diagram, using ULTRACAL for modelling the available experimental c_p-T data.

For this system we have used c_p-T graphs of just five samples, in combination with the thermodynamic properties of the pure substances (table 1) and the excess enthalpy of melting (table 3). Guided by the ULTRACAL results obtained for (1,4-dichlorobenzene + 1,4-dibromobenzene), the experimental c_p-T graphs were used to make a first estimate for the solid–liquid T_x phase diagram: liquidus and solidus temperatures were read from the graphs and used to construct a complete phase diagram. In order to obtain a thermodynamically correct phase diagram, we have used TXFIT,⁽¹⁴⁾ a computational procedure for the direct derivation of excess properties from experimental phase diagram data. When both the liquidus and the solidus are known and used as input to TXFIT, $G^{E,s}$ as well as $G^{E,l}$ can be calculated. Hence, there are four adjustable parameters: g_0^l , g_1^l , g_0^s , and g_1^s , *i.e.* the parameters of the two excess functions of equation type (3). The output phase diagram of TXFIT is subsequently used as input for ULTRACAL. After minimization of the difference between the experimental and the calculated c_p-T graphs (by varying the dispersion for each of the calculated graphs), the experimental and calculated c_p-T graphs are compared, and the deviations used to correct the solidus and liquidus temperatures. Subsequently a new iteration is started.

TABLE 5. Temperatures of inflexion points at rising and falling edges of c_p-T graphs, denoted by T_i^{sol} and T_i^{liq} , respectively. The solidus and liquidus temperatures that correspond to the optimized phase diagram of (1,4-dichlorobenzene + 1,4-dibromobenzene) and the ULTRACAL phase diagram of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) are given for comparison; these temperatures were calculated for the mean composition x_m of the sample and are denoted by $T_{\text{calc}}^{\text{sol}}$ and $T_{\text{calc}}^{\text{liq}}$, respectively. The inflexion point temperatures fall into two categories that are distinguished by roman and italic printing

x_m	$T_i^{\text{sol}}/\text{K}$	$T_{\text{calc}}^{\text{sol}}/\text{K}$	$T_i^{\text{liq}}/\text{K}$	$T_{\text{calc}}^{\text{liq}}/\text{K}$
(1,4-dichlorobenzene + 1,4-dibromobenzene)				
0.21	327.77	327.83	329.09	329.40
0.52	333.58	333.95	341.74	342.02
0.59	336.59	336.33	344.95	345.25
0.60	336.46	336.50	345.55	345.46
0.81	346.54	346.45	353.90	353.90
0.83	346.98	347.30	354.45	354.42
(1,3,5-trichlorobenzene + 1,3,5-tribromobenzene)				
0.20	340.10	340.18	347.46	346.86
0.40	345.46	345.66	364.21	362.46
0.50	349.40	349.24	369.35	369.28
0.68	358.58	358.55	379.15	379.76
0.81	369.55	368.27	385.90	386.30

Four iterations were sufficient to obtain a good match between the experimental and calculated c_p-T graphs. The results consist of (i) calculated c_p-T graphs (figure 5), (ii) obtained dispersions (table 4), (iii) calculated phase diagram (figure 6 and table 2), and (iv) values of the adjusted excess Gibbs energy parameters: $g_0^l = 424 \text{ J} \cdot \text{mol}^{-1}$, $g_1^l = -142 \text{ J} \cdot \text{mol}^{-1}$, $g_0^s = 1980 \text{ J} \cdot \text{mol}^{-1}$, and $g_1^s = 254 \text{ J} \cdot \text{mol}^{-1}$.

DETERMINATION OF PHASE DIAGRAMS WITHOUT ULTRACAL

Inspection of the results presented in figures 4 and 5 reveals that the ideal c_p-T graphs and the experimental data generally intersect at the points where the rising and falling edges of the experimental graphs have their maximum slopes. Taking this into account, and given the fact that an ideal c_p-T graph has infinite (that is to say, maximum) slopes at the solidus and liquidus temperatures of the phase diagram, it seems realistic to assume that

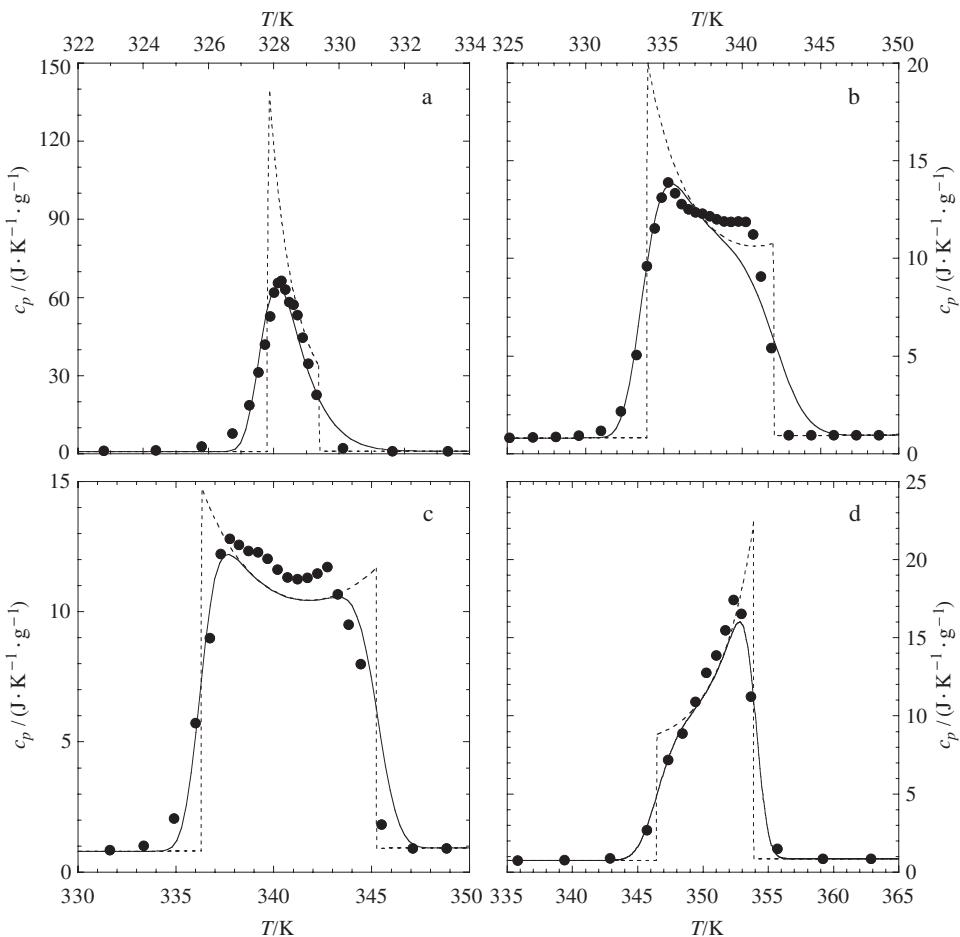


FIGURE 4. c_p-T graphs of four samples with mean compositions $x_m = 0.21$ (a), $x_m = 0.52$ (b), $x_m = 0.60$ (c), and $x_m = 0.81$ (d) of (1,4-dichlorobenzene + 1,4-dibromobenzene). Apart from the sample with $x_m = 0.60$, which was prepared by zone levelling, all samples were prepared by co-precipitation from solution: ●, experimental data; ---, ideal c_p-T graph; —, c_p-T graph calculated by means of ULTRACAL. See table 4 for corresponding dispersions (σ). Calculations were performed with heat capacity expressed in $\text{J} \cdot \text{K}^{-1} \cdot \text{g}^{-1}$. In this way the error due to conversion of the experimental heat capacity data to $\text{J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$ using the average molar mass can be avoided.

the maximum slopes, at the edges of the c_p-T graph of a real sample, will be observed for the solidus and liquidus temperatures of the mean composition. Mathematically, maximum slopes correspond to points of inflection and for this reason it is worthwhile finding out how close the inflection point temperatures (read from the c_p-T graphs) are to the real solidus and liquidus temperatures.

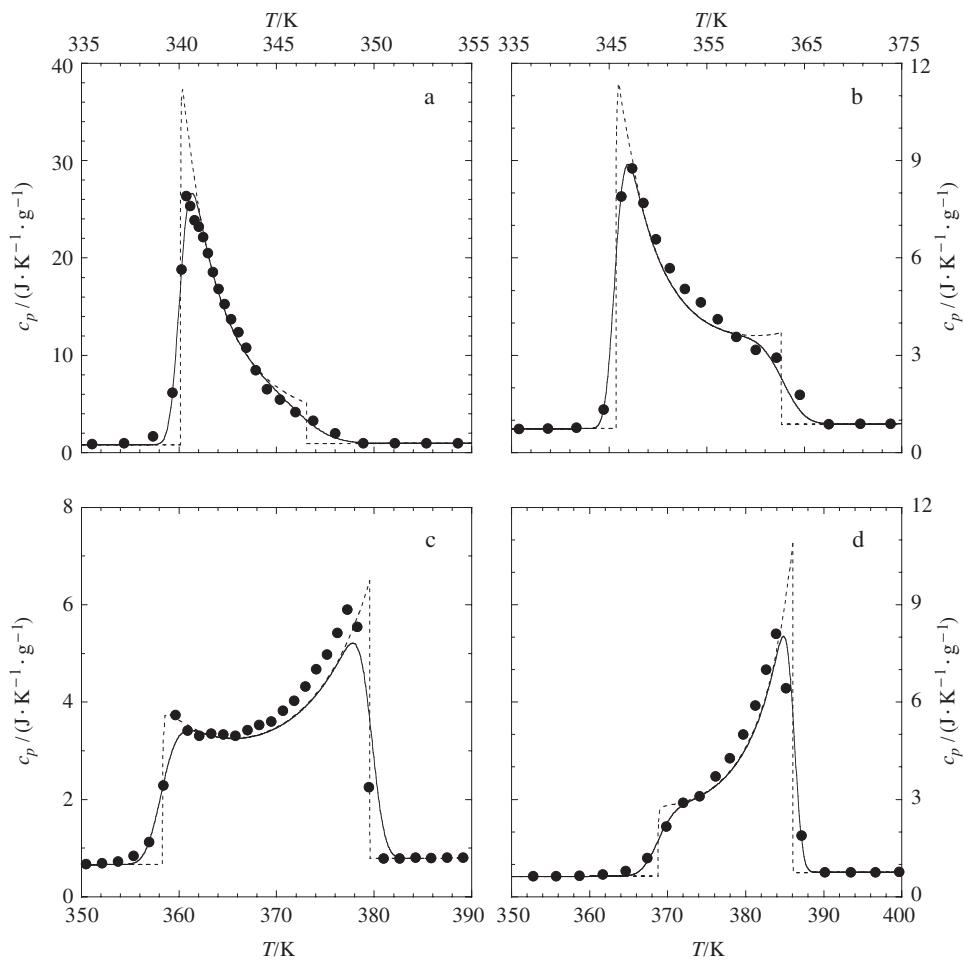


FIGURE 5. c_p-T graphs of four samples with mean compositions $x_m = 0.20$ (a), $x_m = 0.40$ (b), $x_m = 0.68$ (c), and $x_m = 0.81$ (d) of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene). All samples were prepared by co-precipitation from solution: ●, experimental data; ---, ideal c_p-T graph; —, c_p-T graph calculated by means of ULTRACAL. See table 4 for corresponding dispersions (σ). Calculations were performed with heat capacity expressed in $\text{J} \cdot \text{K}^{-1} \cdot \text{g}^{-1}$. In this way the error due to conversion of the experimental heat capacity data to $\text{J} \cdot \text{K}^{-1} \cdot \text{mol}^{-1}$ using the average molar mass can be avoided.

The inflection point temperatures at the rising and falling edges were derived geometrically from the experimental c_p-T graphs. The results are given in table 5, where the solidus and liquidus temperatures derived from the calculated phase diagrams are noted for comparison.

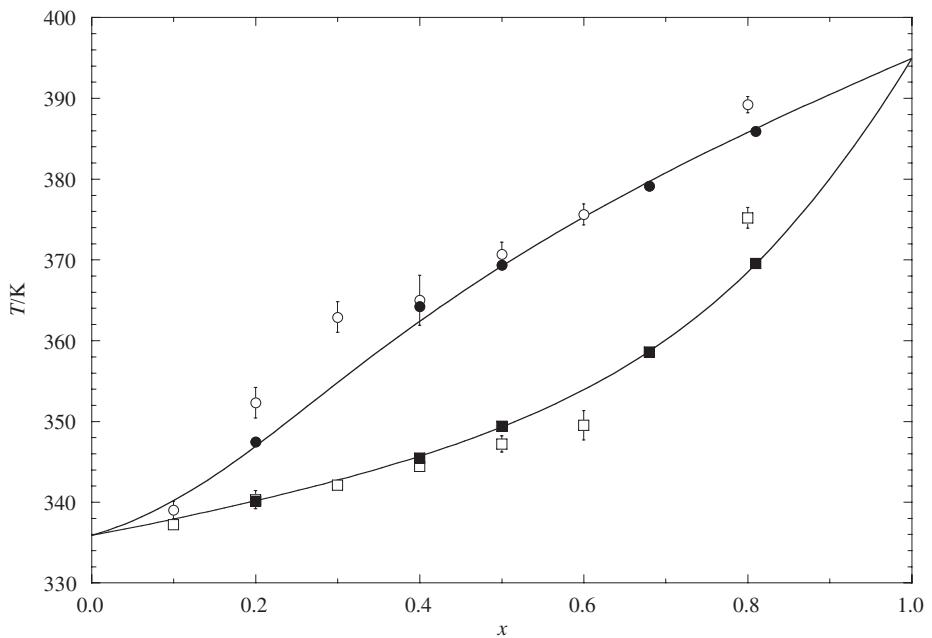


FIGURE 6. Solid–liquid T_x phase diagram of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene): ●, inflexion point at the falling edge of the c_p-T graph; ■, inflexion point at the rising edge of the c_p-T graph; ○, liquidus data by Maiga;⁽¹⁵⁾ □, solidus data by Maiga;⁽¹⁵⁾ —, phase diagram calculated using excess Gibbs-energy functions in terms of the parameters of equation (3): ($g_0^1/J \cdot mol^{-1}$) = 424, ($g_1^1/J \cdot mol^{-1}$) = -142, ($g_0^s/J \cdot mol^{-1}$) = 1980, and ($g_1^s/J \cdot mol^{-1}$) = 254 and the data listed in table 1 (in the calculations the temperature dependence of the transition heat capacity of the pure substances was not taken into account).

6. Discussion

THE ULTRACAL MODEL

According to figures 4 and 5, the reproduction by ULTRACAL of the experimental c_p-T data, although not complete, is good. Considering the obvious limitations of the underlying model, in particular the fact that there is only one adjustable parameter (σ), the results are more than satisfactory. This indicates that the basic assumptions are quite realistic. In other words, the model provides evidence on the existence of a Gaussian distribution of compositions and on the independent melting of the crystallites (at least in the initial stage). However, evidence is no proof and we limit ourselves therefore to the observation that σ , a measure for the degree of inhomogeneity, should approach the value of zero for mole fractions approaching $x = 0.0$ or $x = 1.0$. As can be seen in figure 7, our results basically satisfy this *a priori* condition.

From a comparison of figures 4 and 5 it follows that the c_p-T graphs for the unknown phase diagram of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) are equally well

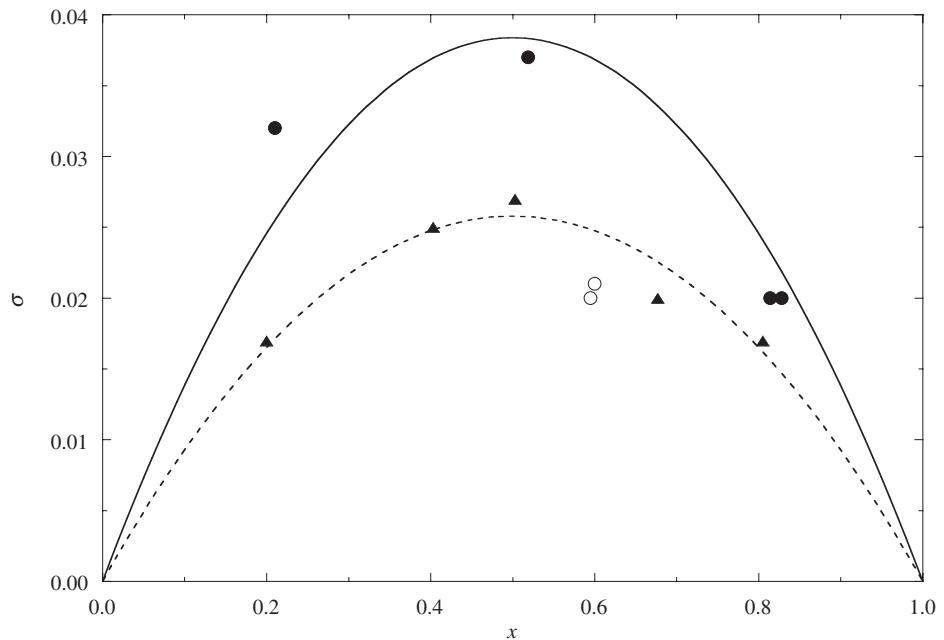


FIGURE 7. Plot of dispersion σ as a function of the mean composition x_m of the samples: ●, (1,4-dichlorobenzene + 1,4-dibromobenzene) samples prepared by co-precipitation from solution; ○, (1,4-dichlorobenzene + 1,4-dibromobenzene) samples prepared by zone levelling; ▲, (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) samples prepared by co-precipitation from solution; —, (1,4-dichlorobenzene + 1,4-dibromobenzene) fit of the dispersion for the samples prepared by co-precipitation from solution: $\sigma(x) = (0.153 \pm 0.012) \cdot x \cdot (1 - x)$; ---, (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) fit of the dispersion: $\sigma(x) = (0.103 \pm 0.003) \cdot x \cdot (1 - x)$.

reproduced as those of (1,4-dichlorobenzene + 1,4-dibromobenzene) for which the phase diagram was known and used as input in the computational procedure. It must be noted that the determination of the dispersion and simultaneous determination of the solidus and liquidus temperatures may show some interdependence.

THE INFLEXION POINT TEMPERATURES

In table 5 two categories of inflexion point temperatures for (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) can be distinguished. The three temperatures in italics correspond to edges of the c_p-T graphs, such as the falling edge in figures 5(a) and 5(b), where the inflexion point is not clearly discernible. The temperatures of the other category correspond to edges in the c_p-T graph where the slope is steep and as a result the point of inflection can be determined with precision, that is to say within ± 0.05 K. In the latter case the absolute average deviation between the calculated and inflexion point temperatures is just 0.22 K. On the basis of this result it can be concluded that, within the experimental errors, the inflexion point temperatures coincide with the solidus and

liquidus temperatures of the phase diagram. The fact that the deviations are larger for the inflexion point temperatures in italics does not contradict this conclusion.

In the case of (1,4-dichlorobenzene + 1,4-dibromobenzene) the situation is different: the phase diagram used to make the comparison is fully independent of the experimental c_p-T graphs. It means that any differences between the phase diagram and inflexion point temperatures will also reflect a disagreement between the original phase diagram and the phase diagram that would have been obtained if the same procedure applied to (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) was used. In other words, the differences between inflexion point and calculated temperatures, as displayed in table 5, may also have, apart from one random, a systematic component. As for the latter, both the solidus and liquidus inflexion point temperatures are, on the average, about 0.10 K lower than the temperatures of the calculated diagram. If a correction of -0.10 K is applied, the absolute average deviation between the inflexion point temperatures and the phase diagram reduces to 0.10 K.

ACCURACY AND PRECISION OF SOLIDUS AND LIQUIDUS TEMPERATURES

In experimental phase diagram research on molecular mixed crystals the work by Campbell and Prodan⁽⁹⁾ on (1,4-dichlorobenzene + 1,4-bromochlorobenzene + 1-bromo-4-chlorobenzene) and its binary subsystems constitutes a major contribution. By means of a thermodynamic phase diagram analysis it can be shown⁽¹⁰⁾ that their liquidus temperatures have a high precision (absence of random errors), the absolute average deviation being 0.10 K. From the mutual consistency of the two sets of experimental liquidus temperatures, see figure 3, it follows that the accuracy (absence of systematic errors) of Campbell and Prodan's liquidus points is also high. The systematic error is estimated to be ± 0.10 K at most.

Prior to the present investigation, our opinion was that the 0.10 K-level for liquidus temperatures and *a fortiori* for solidus temperatures could only be reached by adiabatic calorimetry in combination with zone levelling for the preparation of samples. At the end of the investigation we have arrived at the conclusion that practically the same level can be reached when zone levelling is replaced by rapid co-precipitation from solution.

PHASE DIAGRAM OF (1,3,5-TRICHLOROBENZENE + 1,3,5-TRIBROMOBENZENE)

In figure 6 the solid-liquid T_x phase diagram of (1,3,5-trichlorobenzene + 1,3,5-tribromobenzene) determined using ULTRACAL is shown along with the data of Maïga.⁽¹⁵⁾ These data, determined by means of d.t.a., show a rather erratic path which may be explained by limitations of the experimental technique.

Our phase diagram shows the existence of an uninterrupted series of mixed crystals. Maïga,⁽¹⁵⁾ however, concluded that there would be a solid state miscibility gap manifested by a phase diagram with a peritectic three-phase equilibrium. For this reason it is worthwhile having a closer look at the mixing properties. Restricting ourselves to the equimolar composition, the following data can be derived from the results obtained in this work: $\{\Delta_S^1 H^E(x = 0.5)\} = -1427 \text{ J} \cdot \text{mol}^{-1}$ (see table 3) and $\{G^{E,s}(x = 0.5)\} = 495 \text{ J} \cdot \text{mol}^{-1}$. Assuming that (i) the molar excess enthalpy difference can be attributed

to the solid state, and (ii) the excess properties apply to the mean temperature of the solid–liquid two-phase region, $(T/K) \approx 360$, it can be estimated that the top of the region of demixing is below $(T/K) \approx 225$. At any rate, the conclusion that at room temperature miscibility in the solid state will be complete is justified. Moreover, from a crystallographic point of view complete miscibility is expected in view of the elevated value of the coefficient of crystalline isomorphism ($\varepsilon_m = 0.91$).⁽¹⁵⁾

7. Conclusions

In this study mixed crystalline samples were prepared by the method of rapid coprecipitation from an evaporating solvent. For these samples the solid to liquid transition was measured by means of adiabatic calorimetry and the resulting c_p-T graphs were analysed by means of the ULTRACAL model.

On the basis of the evidence presented in this work, the following conclusions can be drawn: (i) the ULTRACAL model is appropriate for the simulation of experimental c_p-T graphs obtained by adiabatic calorimetry, (ii) the ULTRACAL model can be used to determine the solid–liquid T_x phase diagram from a limited set of c_p-T graphs, and (iii) the inflection points on the rising and falling edges of experimental c_p-T graphs are virtually at the solidus and liquidus temperatures of the solid–liquid T_x phase diagram.

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